

Geotechnical Engineering • Engineering Geology

# **Geotechnical Investigation Work Plan**

# Waste Disposal, Inc. Superfund Site Redevelopment

Santa Fe Springs, California



Prepared for:

Revita WDI, LLC 2050 S. Bundy Drive, Suite 225 Los Angeles, CA 90025

Prepared by:

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December 3, 2008 Project No. REV 07-01E



Mr. Greg Walden Revita WDI LLC 2050 S. Bundy Drive, Suite 225 Los Angeles, CA 90025

Subject:

GEOTECHNICAL INVESTIGATION WORK PLAN

Waste Disposal, Inc. Superfund Site Redevelopment

Santa Fe Springs, California

Dear Mr. Walden:

KFM GeoScience is pleased to submit this Work Plan describing the scope of the proposed geotechnical investigation for the redevelopment of the Waste Disposal, Inc. Superfund Site in Santa Fe Springs, California. The purpose of this Work Plan is to present strategies and methods of obtaining sufficient geotechnical data for the basis of the design for the site redevelopment as well as improvements within the development.

We appreciate the opportunity to provide our professional services on this project. If you have any questions regarding this report or if we can be of further service, please do not hesitate to contact the undersigned.

Respectfully submitted,

KFM GeoScience

Peter Skopek, Ph.D., G.E. 2635

Principal Engineer

Filename: WDI Geotechnical Work Plan.doc

Distribution: Addressee (pdf by email gwalden@revitadev.com)

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### 1. INTRODUCTION

KFM Geoscience (KFMg) has been retained by Revita WDI, LLC to prepare geotechnical designs for the redevelopment of the Waste Disposal Inc. (WDI) site in Santa Fe Springs, California (Figure 1). Revita intends to redevelop the WDI site while complying with the major components of the existing Amended Record of Decision (AROD). As part of the design process it is critical that sufficient geotechnical data be gathered to provide a basis for the design of the overall proposed development as well as for the individual improvements within the development. This Geotechnical Investigation Work Plan has been prepared to address that need.

# 1.1. Site Location and Description

The WDI Superfund site is located in the City of Santa Fe Springs, on approximately 38 acres of land divided into multiple parcels. The site consists of 22 individual parcels of land that are owned by as many as 20 landowners. Owners and tenants operate roughly 35 on-site small businesses around the perimeter of the site. A high school with athletic fields is located immediately adjacent to the northeast corner of the site. A residential area is located across the street to the east.

The site was previously used as a disposal site for oil field wastes and has been the subject of extensive site investigation activities. Based on the results of site investigation activities, a site remedy was developed that included:

- > Capping of portions of the site, near its center with a Resource Conservation and Recovery Act (RCRA) Subtitle C-equivalent cap;
- > Capping of other portions of the site with variations of a RCRA Subtitle D-equivalent cap:
- > Extraction of subsurface gas from the center portion of the site and venting of subsurface gas in other portions of the site;
- > Extraction of liquids from the center portion of the site;
- > Ongoing long term soil gas and groundwater monitoring.

A more detailed description of the history of the WDI site, investigations conducted, and implemented remedy elements is provided in Section 2.0. A site plan showing current site conditions is included as Figure 2. Copies of the As-built Plans for the site remedy are included in Appendix A

## 1.2. Project Objectives

The purpose of this geotechnical investigation described in this Work Plan is to collect sufficient field data to allow for the geotechnical design and construction of proposed site improvements.

## 1.3. Project Organization

All work for this investigation will be performed by KFMg personnel and KFMg subcontractors (testing laboratory, drillers, contractors, suppliers, etc.). The activities described in this Geotechnical Investigation Work Plan will be overseen by Mr. Peter Skopek, Ph.D., G.E. The primary contact for Revita WDI, LLC will be Mr. Greg Walden. Revita is being supported in the overall redevelopment design by Bryan A. Stirrat & Associates (BAS). Mr. Greg Acosta, P.E. and Mr. Kevin Fellows, P.E. of BAS will be available as resources to KFMg in the implementation of this Work Plan.

The WDI Potentially Responsible Parties Group (WDIG) will be represented on this project by Project Navigator Limited (PNL). Mr. Ken Floom will be the primary project contact at PNL. Regulatory oversight will be provided by USEPA Region IX with support from the California Department of Toxic Substances Control (DTSC). The USEPA Project Manager is Mr. Russell Mechem. The DTSC primary reviewers are Ms. Jessy Fiero, Mr. Ram Ramanujam, and Mr. Steve McAdrle. The Corps of Engineers is represented by Mr. John Erwin. The involved parties can be reached as follows:

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### 2. SITE BACKGROUND AND PROPOSED DEVELOPMENT

# 2.1. Site Background

As stated previously, the WDI Superfund site is located in the City of Santa Fe Springs, on approximately 38 acres of land divided into multiple parcels. The site consists of 22 individual parcels, owned by as many as 20 landowners. Owners and tenants operate roughly 35 on-site small businesses around the perimeter of the site. A high school with athletic fields is located immediately adjacent to the northeast corner of the site. A residential area is located across the street to the east.

At its center, the WDI site contains a buried circular earthen perimeter berm concrete-lined 42-million gallon reservoir originally constructed for storage of crude petroleum. The reservoir (also referred to as "the Dial") was decommissioned in the late 1920s, with the site being used until the mid-1960s for disposal of a variety of hazardous substances including both liquid and solid wastes. Wastes disposed of at the site include petroleum-related chemicals, solvents, sludges, construction debris, drilling muds, and other waste materials. Historical aerial photographs show that liquids were discharged to the reservoir and into some areas surrounding the reservoir. The reservoir and portions of the site area were covered with soil during the 1960s. Soil borings indicate that the reservoir is covered by five to ten feet of fill soil. The 15,000 residents of Santa Fe Springs obtain drinking water from wells within 3 miles of the site. The closest residence is within 50 yards of the site.

In 1984 and 1985, testing by the City of Santa Fe Springs detected numerous hazardous substances, including benzo(a)pyrene, phenol, benzene, and toluene, in materials at the facility at depths of as much as 22 feet below ground surface (bgs). Groundwater occurs at a depth of approximately 50 feet bgs.

In 1988 EPA erected a fence around the site to limit the potential for direct contact with site contaminants, and placed multilingual signs at the site to inform the public of potential health risks.

In 1988 and 1989, EPA conducted a remedial investigation (RI) to determine the nature and extent of contamination at the site and to identify possible long-term cleanup actions. The 1989 RI Report concluded that the main potential source of contamination was the reservoir; however, it also identified areas outside of the reservoir that were potential sources of subsurface contamination at the site. The RI Report confirmed the observation form the aerial photographs and concluded that several areas surrounding the reservoir were used as unlined containment ponds for waste disposal and that other areas may have been contaminated by the migration of subsurface liquid wastes or gases.

Late in 1993, EPA issued a Record of Decision (ROD) that selected an environmental remedy to address soils and subsurface gas at the site. This remedy consisted of installing a hazardous waste cap, with gas extraction and treatment, if necessary. The purpose of the capping systems

was to isolate the waste material from direct human contact and minimize the potential for surface water infiltration and prevent the release of any soil vapor to the atmosphere.

After the 1993 Record of Decision was signed and the design of the remedy was underway, new information about the extent of contamination at the site became available. Between 1997 and 1999, EPA and the Waste Disposal, Inc. Group (WDIG), an oversight group formed to investigate, plan for and implement a final remedy for the site, renewed site investigation activities to further define the limits and characteristics of the waste material buried at the WDI site, the extent of subsurface liquids, and the extent of subsurface gas in the reservoir and surrounding areas. Information gathered in these Remedial Design (RD) investigations was used to reevaluate and revise the remedial design for the site. Results of these investigations indicated that an estimated 80% of the site contained buried waste at depths ranging from 5-30 feet, and that buried wastes are present underneath many of the buildings located around the perimeter of the site. The reservoir contained pockets of liquid waste and some of the buried wastes outside of the reservoir also contain liquids. Soil gas investigations revealed the presence of benzene, vinyl chloride, trichloroethene (TCE), and tetrachloroethene (PCE) and methane in subsurface gases. Elevated levels of these contaminants were detected both inside the reservoir and in localized areas outside of the reservoir, including near some on-site buildings. Boring logs from the investigations also identified construction and demolition (C&D) debris are present beneath the site and that the dike that had been constructed along the northern property boundary contained a significant amount of C&D debris.

The WDIG completed a Remedial Design Investigative Activities Summary Report in May 2001. The report summarized the key findings of recent and past investigations conducted at the site. Using the information from investigations performed at the site, the WDIG prepared a Supplemental Feasibility Study (SFS), which evaluated a variety of remedial alternatives for the site. Based on the results of the SFS, EPA developed a preferred alternative for site cleanup. The preferred alternative was presented to the public and community for comment in the Proposed Plan, which was issued as a Fact Sheet in May 2001. EPA held a public comment period on the Proposed Plan from June 1, 2001 to July 2, 2001 and accepted comments on the preferred alternative in writing and orally. EPA also conducted a public hearing on June 14, 2001 in Whittier, California.

The AROD was signed one year later in June 2002, presenting a selected remedy with the following major components:

- 1. Installation of a RCRA-equivalent cap for hazardous waste over the existing reservoir (the Dial);
- 2. Installation of engineered capping systems for areas outside the reservoir designed to achieve RCRA solid waste engineering and performance standards (hydraulic conductivity of 10<sup>-6</sup> cm/sec), and consisting of graded soil monofill covers, asphalt, concrete paving, and/or building foundations;

- 3. Installation of a gas collection, extraction, and treatment system beneath the RCRA-equivalent cap over the reservoir to collect, remove and treat subsurface gases;
- 4. Installation of liquids collection systems including liquids collection points (LCPs) in the reservoir, to monitor, collect and extract leachate and free liquids for treatment and disposal at an off-site facility approved by EPA;
- 5. Use of engineering controls (e.g. physical barriers and/or indoor venting systems) as needed within existing and new buildings overlying or adjacent to waste to prevent exposure to site contaminants;
- 6. To minimize the potential exposure to soil gas, passive gas migration control (e.g. bioventing wells) or active soil vapor extraction systems were installed along portions of the waste perimeter outside the reservoir area and near existing building with monitoring systems installed to ensure performance;
- 7. Implementation of institutional controls (ICs), including zoning ordinances, access controls, groundwater use restrictions, and restrictive covenants, ensuring the integrity of remedial systems, minimize the potential for exposure to residual wastes and hazardous substances, and to restrict land use and site access.
- 8. Implementation of long-term groundwater monitoring to ensure that the revised remedy is not contributing to exceedances of groundwater standards; and
- 9. Implementation of long-term operations and maintenance (O&M) to ensure that all environmental systems and control components are functioning effectively.

The WDIG prepared the engineering design package for the environmental remedy and EPA approved the final package in June 2003. The RD encompassed the remedial components specified in the AROD. The remedial design uses several types of engineered capping systems, including (1) a highly protective, multi-layered RCRA Subtitle C-equivalent cap for the Dial area, (2) a multi-layered RCRA Subtitle D-equivalent cap overlying waste materials outside of the dial, and (3) asphalt and concrete RCRA Subtitle D-equivalent capping materials surrounding existing buildings in the site perimeter. Much of the central portion of the site is topped with a grassy, vegetative soil cover sloped to prevent ponding of water and facilitate surface water drainage. The design includes stormwater and sediment control features. The RD also included an active soil vapor gas collection and treatment system employing a central pumping system to pump soil gas through a star-shaped, radial pipeline system to a treatment system located at the center of the dial. The treatment system consists of a small granular activated charcoal filtration system. For work close to existing buildings, the WDIG developed parcel-specific Work Plans describing the procedures for installing asphalt and/or concrete capping materials for each parcel. The design also called for construction work inside existing buildings to seal cracks and improve floor materials so that existing foundations could serve as capping material.

WDIG began remedial action construction in March 2004 and proceeded in accordance with the approved remedial design. EPA provided coordination with federal, state, and municipal agencies which have interests or oversight roles at the site. EPA established an interagency committee that reviewed project planning and design deliverables and provided oversight during construction. The EPA also contracted with the U.S. Army Corps of Engineers (USACE) to provide field oversight and inspection services during the construction phase of the project.

EPA and USACE determined that the WDIG construction team successfully completed the following key activities during construction of the remedy:

- Excavation and re-compaction of contaminated soil and other unsuitable materials under the new landfill cover in order to achieve design-specified contouring and grade levels.
- Reconditioning of large quantities of existing buried construction debris and large chunks of concrete for cost-effective use in building the cover foundations.
- ▶ Backfilling excavated areas with suitable materials.
- Installation of geosynthetic materials (e.g., geosynthetic clay liner and HDPE geomembrane (RCRA Subtitle C-equivalent cap only) that function as barrier components in the RCRA-equivalent final covers.
- > Implementation of engineering controls, i.e., crack-sealing of parcel-specific building foundations that will serve as final covers.
- > Installation of asphalt and concrete RCRA-equivalent covers in commercial areas on the site.
- Installation of landfill gas extraction and treatment systems for the area overlain by the RCRA-C equivalent cover.
- ➤ Initial revegetation and landscaping of final covers and areas directly adjacent to the neighboring high school. EPA approved the Combined Remedial Action & As-Built Report on September 14, 2006. Operations of the gas extraction and treatment systems in were initiated in March 2005.

The WDIG is currently conducting on-site activities in accordance the Long Term Operations, Maintenance and Monitoring Plan for the Site approved by EPA on September 21, 2006. These activities include:

- > Routine Inspections Routine inspections of the engineered caps and all site systems.
- > Cap Maintenance Routine maintenance and repair of RCRA-equivalent, asphalt and concrete engineered capping systems.
- Maintenance of Soil Vapor Collection & Treatment Systems Routine inspection, maintenance and repair of soil vapor wells, air monitoring systems, and soil vapor collection and treatment systems.
- Collection & Extraction of Liquids from the Reservoir Bailing and later installation of low-volume pumping systems to remove very low volumes of liquids from the central reservoir area ("dial"). Liquids are shipped offsite to an EPA-approved hazardous materials treatment facility.

- Maintenance of Vegetative Cover Inspections, mowing, and hydroseeding of vegetative soil cover to help maintain and protect the integrity of the cap, control stormwater run-off, and maintain a natural appearance.
- > Stormwater & Sedimentation Control Features Inspection and repair of stormwater and sediment control systems (swales, berms, retention structures, etc.).
- ▶ Landscaping Periodic mowing, pruning, and weeding of site vegetation.
- ➤ General housekeeping General site maintenance.
- ➤ Long Term Groundwater Monitoring Semi-annual collection and analysis of samples of groundwater at the site and semi-annual reporting to EPA.
- > Long Term Soil Vapor Monitoring Quarterly sampling and analysis with semi-annual reporting.
- ➤ Long Term Indoor Air Monitoring Quarterly monitoring at indoor air monitoring locations at the site with semi-annual reporting.
- > Corrective Action Identification and implementation of corrective actions as determined necessary by EPA.

With funding from EPA, the City of Santa Fe Springs prepared a formal specific use plan for the WDI site. EPA and the WDIG coordinated with the City throughout the planning process to help maintain consistency between the remedial design and the City's land use plan. The City's municipal council adopted the WDI site Specific Use Plan on May 13, 2004. The plan prohibits future residential land uses and provides guidelines and requirements regarding future industrial redevelopment at the site. It also places certain restrictions and land use controls that are intended to help protect the environmental remedy.

## 2.2. Proposed Development Elements

The current proposed WDI Site development encompasses only the central portions of the WDI site as depicted on conceptual site development plan included as Figure 2-1. The total proposed development area is 20.4 acres with access being from Santa Fe Springs Boulevard on the west and Greenleaf Avenue on the east. As shown in the conceptual plan, the proposed development will include hardscaped, at-grade yards across the majority of the site. Almost all of these areas are underlain by waste material with either a Subtitle-C equivalent cap or Subtitle-D equivalent cap as described in Section 2.1.

Perimeter retaining walls will be required around the majority of the site to allow for proper drainage. The two most significant of these walls will be along the north property boundary, where the cantilever retaining wall height may vary from 8 to 14 feet and support 6- to 8-foot screen wall; and along the west property boundary in the northwest corner, where the wall height is anticipated to be 8 feet. The north wall alignment is underlain by native material. However, this northern wall is planned to be constructed at the toe of the earthen dike along the northern site boundary that reportedly contains significant amounts of construction and demolition debris. The west wall alignment is predominantly underlain by native material, although fingers of waste may extend beneath the alignment in places. An asphalt overlay acts as the existing cover along the alignment of the proposed western retaining wall.

Shorter walls, with anticipated heights of less than 36 inches are currently planned for the southern and southeast property boundaries. These areas are underlain predominantly by covered waste materials. The cover in these areas is the Subtitle-D equivalent GCL cover described in Section 2.1 along its interface with native material or the asphalt overlay on the adjacent property. Portions of the alignments of these shorter southern and southeastern walls are over native material. However, even in these areas, the GCL material is present.

There is a possibility that the development may include a site building in the northeast corner (as shown in Figure 2-1), constructed entirely outside of the footprint of the deposited waste material. The need for such a building is currently being evaluated by Revita, in consultation with the City.

## 3. GEOTECHNICAL INVESTIGATION APPROACH

# 3.1. Geotechnical Investigation Strategies and Methods

In developing the engineering designs for the proposed site development, the site design team will need to gather sufficient geotechnical information to ensure that a proper basis of design has been established. The activities needed to gather that information are described in this Geotechnical Investigation Work Plan.

As stated previously, the grades at the site will need to be contoured to satisfy drainage requirements. It is expected that up to about 2 to 3 feet of fill will locally be required. For pavement and storage areas the surface cover will either be an asphalt pavement, or in areas with permanent heavy loads (e.g., loading docks, storage) a concrete pavement may be considered. The surface cover design will be based on traffic loading (i.e., dynamic transient load) as well as on conventional structural principles for slabs on grade supporting permanent loading. Consideration will be given to improve the performance of the pavement by placement of geogrids to strengthen the pavement subgrade (e.g., Tensar Dimension system) and to include fiberglass reinforcement within the asphalt pavement section (e.g., Bitutex) or conventional steel reinforcement in the concrete slabs on grade.

Although numerous borings and probes were advanced across the site, with the exception of 13 borings advanced by Lowney (2002) all of them focused on collection of environmental data and are of limited use for geotechnical design. Although the data collected in all borings and probes advanced at the site is being used to develop the understanding of the foundation conditions at the site the design of the proposed improvements within the refuse area requires additional structure-specific investigation of the geotechnical properties of the near surface materials that will support the pavements, slabs-on-grade, and small retaining walls. Proposed improvements outside the refuse areas on native soils which include the larger retaining walls and potential buildings at the site will also require structure-specific investigation of deeper materials. The focus of the geotechnical investigation covered in this work Plan will be to address the following development elements:

- 1. Evaluation of condition of the existing covers and collection of data to determine the properties of the existing cover components as it relates to the design of the pavement and proposed cover in the open, parking, and driveway areas including the proposed surface storage yards.
- 2. Geotechnical design parameters for a retaining wall of up to about 14 feet in height along the northern and northeastern boundary of the project located on native materials.
- 3. Geotechnical design parameters and recommendations for smaller retaining walls located on both native materials and areas underlain by waste along the west, south, and east perimeter of the site required for proper site drainage.
- 4. Geotechnical design parameters and recommendations for the proposed approximately 33,000 square-foot building in the northeast corner of the site located on native materials. (PROVISIONAL).
- 5. Geotechnical design parameters for light poles will be required depending on the location and size of the light standards. (PROVISIONAL)

The details of the proposed scope of investigation, including testing locations, distribution and depth of borings for each of the above elements are summarized in the Geotechnical Investigation Matrix (GIM) -Table 3-1. The proposed geotechnical investigations will consist of drilling deep borings and performing Standard Penetration Testing (SPT) in native non-waste areas, hand-augering shallow borings in cover materials above the low permeability barrier layers, and testing of near-surface compressibility using plate load testing. Approximate locations of these investigations are shown on Figure 3 – Geotechnical Investigation Location Map. The encountered materials will be logged and tested in the field and sampled for subsequent laboratory testing. Laboratory testing will focus on classification, plasticity, gradation, strength, compressibility, and permeability properties of the field materials.

The following paragraphs address some specific aspects of the proposed investigation.

> Geotechnical investigation for design improvements located above the Subtitle C- and D-equivalent cover areas will require evaluation of the properties of materials above and below the GCL and GCL/HDPE barrier layers as well as of the properties of the foundation layer, soil cover, and/or refuse materials below the barrier layers. This consideration applies to open, parking, and driveway areas as well as to some of the retaining walls located along the east, south, and west site perimeter.

No penetration of borings and probes into the refuse is intended. Typical investigation activities to be performed in these areas will include:

☐ In the Subtitle C- and D- equivalent cover areas shallow hand-auger borings will be excavated penetrating only into the upper vegetative layer above the low permeability

barrier cover components (GCL and HDPE). The cover will be repaired as outlined in Section 3.1.

- ☐ In the areas along the site perimeter where Subtitle D- equivalent cover is installed where no refuse is indicated according to the as-built plans, the cover will be penetrated into the native materials and the cover will be repaired as outlined in Section 3.1.
- ☐ In areas where alternative covers (asphalt, concrete) are installed where no refuse is indicated according to the as-built plans, the cover will be penetrated into the native materials and the cover will be repaired as outlined in Section 3.1.
- □ In areas above the refuse a non-invasive plate load test, which does not require penetration through the liner components, will be utilized. The plate load test is intended to evaluate the compressibility and uniformity of the near-surface materials without penetrating the CGL or GCL/HDPE liner. The plate-load reaches depths of approximately 2.5 times the plate diameter. As such, and in order to evaluate the properties of the foundation layer below the GCL or GCL/HDPE cover layers, it is proposed that a 12-inch diameter plate be used for the test, and that the base of the plate be set in a shallow excavation of approximately 12 to 18 inches deep. Care will be taken in creating the shallow excavation to ensure that the GCL or GCL/HDPE low permeability layers are not damaged or penetrated. It is intended that the plate will penetrate no more than about 1 inch into the subgrade. Consequently, the strains associated with the barrier layers deflection below the plate are expected to be acceptable. The plate load tests will be performed generally following ASTM Standard D1195 and AASHTO T-222-78.
- ➤ In the northwest corner of the site, a proposed retaining wall is generally located predominantly above native materials (i.e., not above refuse) in areas where the in-place site remedy includes a 2 inch asphalt overlay or concrete cover. Conventional methods of investigation can be implemented in this area and, as necessary, the cover will be repaired as outlined in Section 3.1.
- > A 14-foot retaining wall designed to accommodate grading and stormwater design elements is proposed along the north property perimeter dike. Fill will be placed over the north slope of the perimeter dike and will be supported by the retaining wall. This wall, as well as the toe of the perimeter dike, are located outside of the waste areas but the backcut will require cutting into the dike composed of not well defined materials (previous investigations have indicated this to be construction debris fill). No penetration of the existing final covers is expected in this area and conventional geotechnical investigation methods will be implemented. It is expected that conventional shallow foundation systems will be appropriate for this construction.
- > The construction of a habitable structure in the northeast corner is currently being considered to occur only outside the final cover areas where waste does not exist. Consequently conventional geotechnical investigation methods can be implemented in this area. It is

expected that conventional shallow foundation systems will be appropriate for this construction.

- ➤ A 6-foot retaining wall is considered in the northeast corner of the site to support the pad for the proposed building. This retaining wall is located entirely on native materials therefore it is expected that conventional geotechnical investigation and foundation methods will be implemented.
- > Pending the decision of the design and regulatory team, foundations for light towers and/or poles may be required. The investigation for the foundations for such improvements will highly depend on the actual size and location of the light towers/poles and will be addressed once that decision is made.
- Field equipment not penetrating through the CGL/HDPE liner and/or refuse materials will not need to be decontaminated between test/boring locations or upon departure from the site. Although not anticipated, field equipment penetrating the CGL/HDPE liner and/or refuse materials will not need to be decontaminated between test/boring locations but will be decontaminated upon departure from the site.
- > Repair procedures for excavations in the native areas as well as for all excavations penetrating any component of the existing final cover, including the surficial vegetative layer are provided in Section 3.1.
- > Drill cuttings generated from any on-site drilling operations will be stockpiled and covered with plastic sheeting pending characterization for disposal purposes. Drill cuttings will be transported off-site for disposal per state and federal regulatory requirements. A Health and Safety Plan has been prepared for this work and is provided under a separate cover.

It is expected that the field investigation plan will be modified/finalized upon discussion with EPA and the design team, specifically with the civil engineering designer.

The field investigation scope, collected data, and results of all testing will be summarized in a geotechnical design report including provision of design recommendations for appropriate foundation system, slab on grade design, geogrid reinforcing systems, seismic structural design, and general grading and drainage recommendations.

# 3.2. Repair Procedure When Existing Cover Component is Penetrated

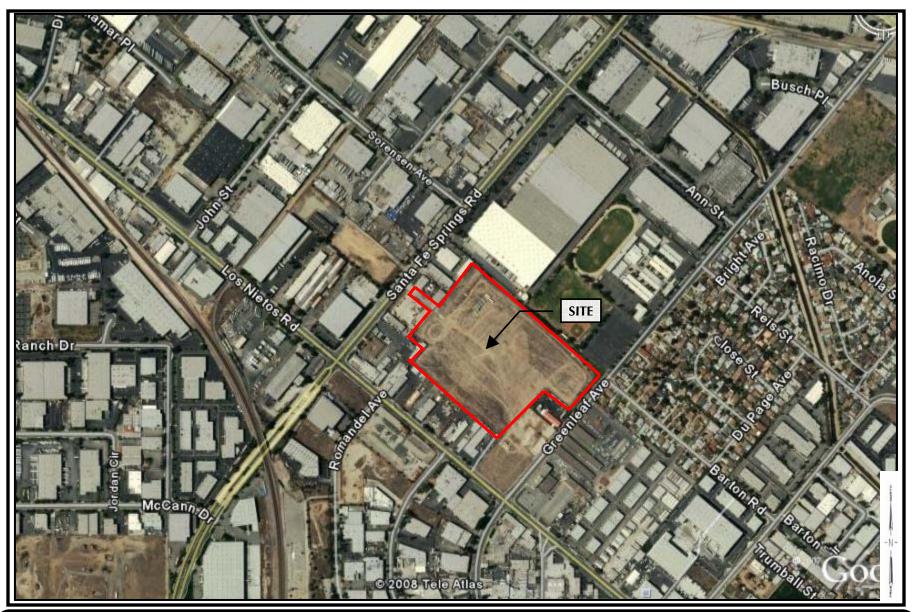
While performing this investigation the following repair protocols will be adhered to:

- a) Penetration of the HDPE cover layer located within the Dial is not permitted and must be avoided.
- b) When the vegetative layer is disturbed during excavation of shallow hand-auger borings or pits for the plate load test not exceeding 5 feet square, or similar excavation not

penetrating HDPE or GCL components, the excavation will be backfilled with either on site material or import soil with at least 25 percent of fines. The backfill will be moisture-conditioned to above optimum moisture content and compacted by hand methods to 85 to 90 percent of maximum dry density as determined by the latest edition of ASTM D1557.

- c) If the GCL layer of the existing Subtitle D-Equivalent cover outside the Dial is penetrated the penetration will be repaired by backfilling a minimum of 1 foot above and below the GCL with a cement-bentonite slurry.
- d) Where the existing asphalt or concrete cover is penetrated, the penetration will be repaired by quick-set high-strength concrete mix to a depth of at least 18 inches below the adjacent grade. The surface of the repair will be blackened, if needed, to better blend with the adjacent cover.
- e) All excavations and borings in the native areas will be backfilled with tamped drill cuttings.

# **FIGURES**





BRYAN A. STIRRAT & ASSOCIATES CIVIL AND ENVIRONMENTAL ENGINEERS 1360 VALLEY VISTA DRIVE, DIAMOND BAR, CA 909-860-7777 Waste Disposal Inc. Site Santa Fe Springs Road & Los Nietos Road Santa Fe Springs, California

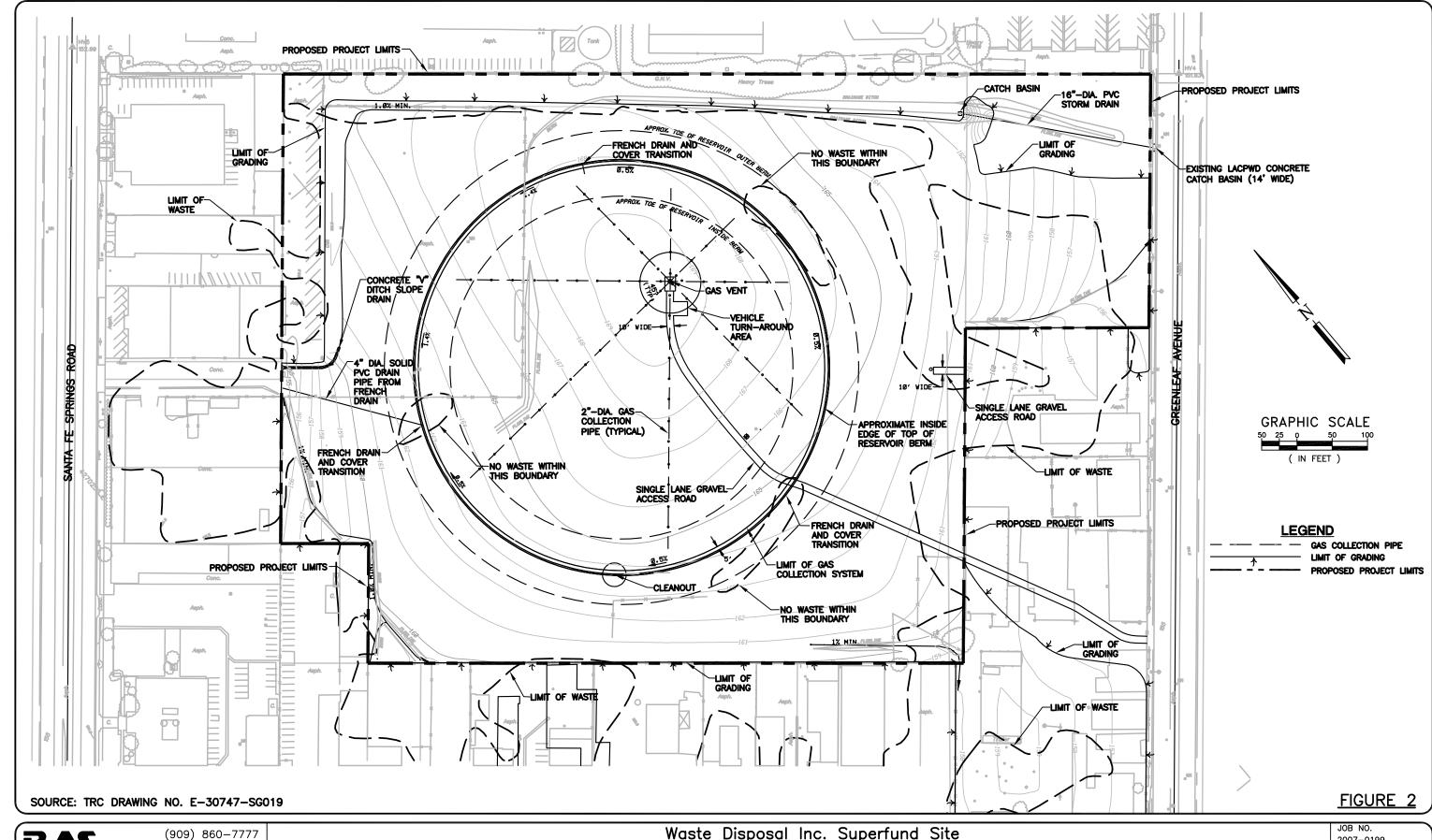
Figure 1
Site Location Map

JOB NO. 2007.0199 Phase 003A

DATE: September 4, 2008

DRAWN BY: K. Hall

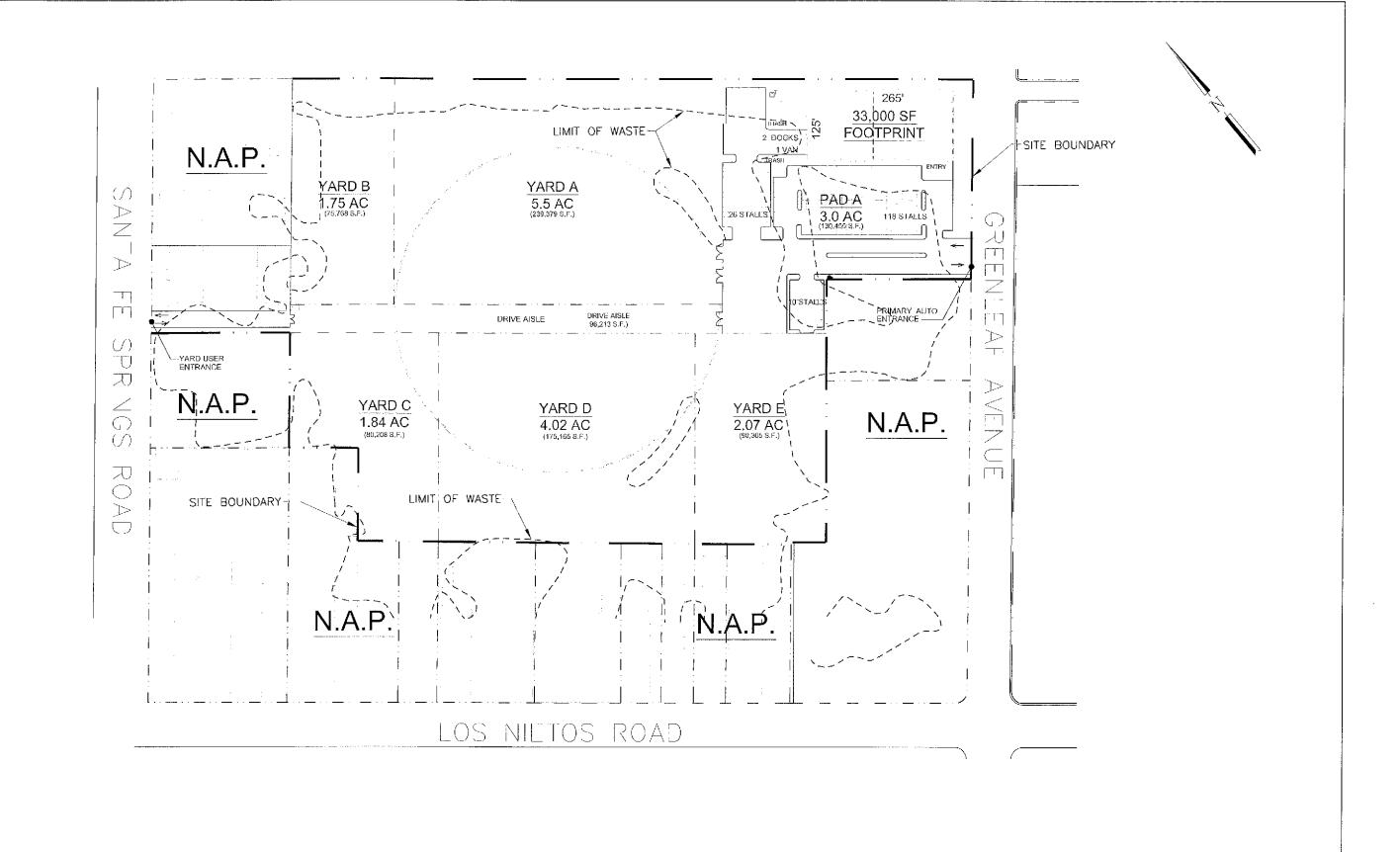
FILE: J:\Revita\WDIG\Work Plan\Figure 1 – Site Location Map



BRYAN A. STIRRAT & ASSOCIATES CIVIL AND ENVIRONMENTAL ENGINEERS 1360 VALLEY VISTA DRIVE DIAMOND BAR, CA 91765 Waste Disposal Inc. Superfund Site

SITE MAP

2007-0199 DATE 9-2-08 DRAWN BY A.R.C. FILE NAME: SITE MAP.DWG



REVISION DESCRIPTION

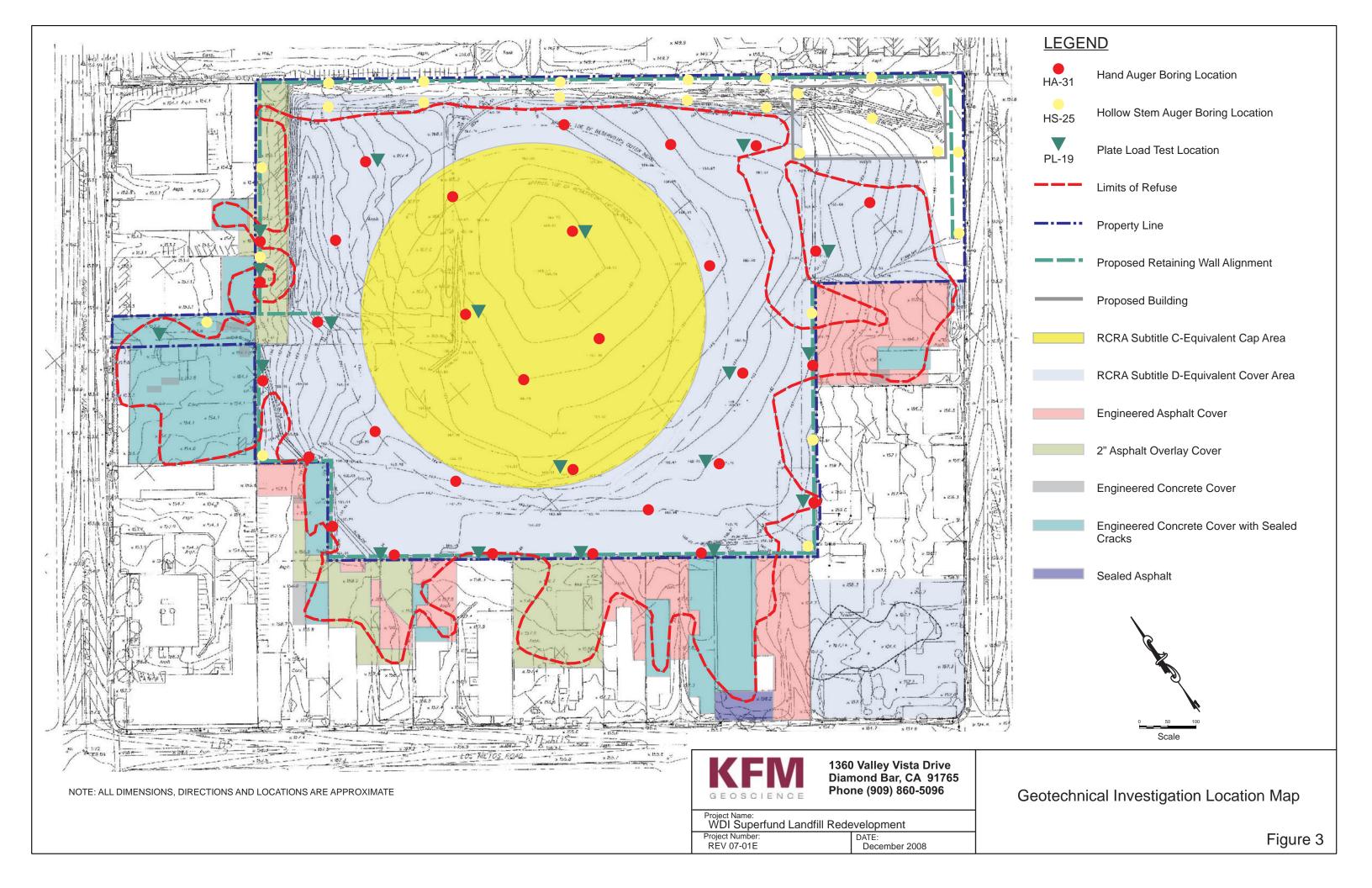
PRELIMINARY DRAFT NOT FOR CONSTRUCTION

BRYAN A. STIRRAT & ASSOCIATES
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# WDI SITE DEVELOPMENT PROJECT SITE DEVELOPMENT PLAN

DESIGNED BY: K.H.F. & G.A.	SCALE : AS SHOWN
DRAWN BY: A.R.C. & F.A.	DAYE : 10-2008 FILE NO.: 2 SITE DEVELOPMEN
CHECKED BY : NAME	DATE : 10-2008
APPROVED BY : B.A.S.	DATE : 10-2008 SHEET 2 OF



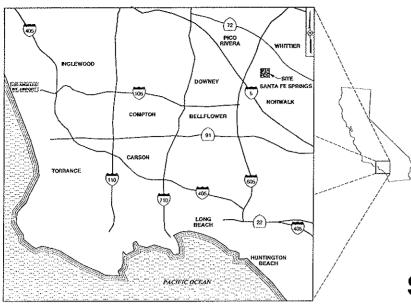
# **TABLES**

SUBJECT SPECIFIC WORK PLAN for AC cover design  Design of surface the proposed sudemonstrate the the existing cover surface Cover in Open Areas (i.e., aspahlt and concrete pavement in site yards)  Pavement/slab- Evaluate subgrasupport intended loads	e percolation rate through sed surface cover and ate the equivalency with ag cover systems  It subgrade load capacity to tended traffic and storage	rater characteristic curve (SWCC) for use HELP model. Specifically, determine atturated (0kPa) hydraulic conductivity (k), and conductivity at field capacity (-33kPa) and at wilting point (-1500kPa)  an-situ soils conditon characterization, noisture content, and density and devalue determination for pavement design	How to Obtain Needed Parameters  SUBJECT TO SCHEDULE ACCORDING TO SEPARATE WORK PLAN	Investigation Activi  Field Investigation  (Repair any disturbance of the cover per workplan; additional specific repair requirements are stated in the matrix)  No field investigation required  Excavate 19 hand-auger borings at locations across the site including Subtitle C and Subtitle D -	Lab Testing  Perform water retention test on 2 AC samples	Engineering Processing of Data  Utilize the obtained SWCC in percolation analyses using HELP computer software
SUBJECT SPECIFIC WORK PLAN for AC cover design  Determine percet the proposed sudemonstrate the the existing cover design of surface.  Surface Cover in Open Areas (i.e., aspahlt and concrete pavement in site yards)  Pavement/slab-evaluate subgrasupport intended loads	surface cover e percolation rate through sed surface cover and ate the equivalency with ag cover systems  In the surface design subgrade load capacity to tended traffic and storage	insaturated flow properties for AC and ingineered subgrade described by soil vater characteristic curve (SWCC) for use in HELP model. Specifically, determine aturated (0kPa) hydraulic conductivity (k), and conductivity at field capacity (-33kPa) and at wilting point (-1500kPa)  in-situ soils conditon characterization, poisture content, and density and devalue determination for pavement design	SUBJECT TO SCHEDULE ACCORDING TO SEPARATE WORK PLAN Prepare sample of characteristic asphalt mix (without Petromat or Bitutex) and perform water retention test  Collect samples of the existing vegetative layer, perform soil characterization, and recompact selected samples to proposed design specifications (93% of maximum dry density at 110% of optimum moisture content) and perform the water retention test	Field Investigation (Repair any disturbance of the cover per workplan; additional specific repair requirements are stated in the matrix)  No field investigation required	Lab Testing  Perform water retention test on 2 AC samples	Utilize the obtained SWCC in percolation analyses using HELP
SUBJECT SPECIFIC WORK PLAN for AC cover design  Design of surface the proposed sudemonstrate the the existing cover surface Cover in Open Areas (i.e., aspahlt and concrete pavement in site yards)  Evaluate subgrasupport intended loads	surface cover e percolation rate through sed surface cover and ate the equivalency with ag cover systems  In the surface design subgrade load capacity to tended traffic and storage	insaturated flow properties for AC and ingineered subgrade described by soil vater characteristic curve (SWCC) for use in HELP model. Specifically, determine aturated (0kPa) hydraulic conductivity (k), and conductivity at field capacity (-33kPa) and at wilting point (-1500kPa)  in-situ soils conditon characterization, poisture content, and density and devalue determination for pavement design	SUBJECT TO SCHEDULE ACCORDING TO SEPARATE WORK PLAN Prepare sample of characteristic asphalt mix (without Petromat or Bitutex) and perform water retention test  Collect samples of the existing vegetative layer, perform soil characterization, and recompact selected samples to proposed design specifications (93% of maximum dry density at 110% of optimum moisture content) and perform the water retention test	(Repair any disturbance of the cover per workplan; additional specific repair requirements are stated in the matrix)  No field investigation required	Perform water retention test on 2 AC samples	Utilize the obtained SWCC in percolation analyses using HELP
PLAN for AC cover design  Design of surface the proposed sudemonstrate the the existing cover in Open Areas (i.e., aspahlt and concrete pavement in site yards)  Evaluate subgras support intended loads	e percolation rate through sed surface cover and atte the equivalency with ag cover systems  It subgrade load capacity to tended traffic and storage	ngineered subgrade described by soil nater characteristic curve (SWCC) for use I HELP model. Specifically, determine aturated (0kPa) hydraulic conductivity (k), nd conductivity at field capacity (-33kPa) nd at wilting point (-1500kPa) situ soils conditon characterization, noisture content, and density andvalue determination for pavement design	Prepare sample of characteristic asphalt mix (without Petromat or Bitutex) and perform water retention test  Collect samples of the existing vegetative layer, perform soil characterization, and recompact selected samples to proposed design specifications (93% of maximum dry density at 110% of optimum moisture content) and perform the water retention test			percolation analyses using HELP
Surface Cover in Open Areas (i.e., aspahlt and concrete pavement in site yards)  Evaluate subgrasupport intended loads	in secolation rate through seed surface cover and ate the equivalency with a g cover systems  It is seed surface cover and an area of the seed surface cover systems  It is seed surface cover and an area of the seed surface cover systems  It is seed surface cover and area of the seed surface cover and area of the seed surface cover and the seed	HELP model. Specifically, determine attracted (0kPa) hydraulic conductivity (k), and conductivity at field capacity (-33kPa) and at wilting point (-1500kPa)  In-situ soils conditon characterization, noisture content, and density and design determination for pavement design	recompact selected samples to proposed design specifications (93% of maximum dry density at 110% of optimum moisture content) and perform the water retention test	Excavate 19 hand-auger borings at locations across the site including Subtitle C and Subtitle D -		
pavement in site yards)  Pavement/slab-  Evaluate subgrasupport intender loads	visiab-on-grade design subgrade load capacity to itended traffic and storage	n-situ soils conditon characterization, noisture content, and density and P-value determination for pavement design	Collect samples of the existing vegetative layer, perform soil characterization. R-	equivalent covers to the liner (GCL, HDPE geomembrane) and perform a field moisture and field density tests (sand cone or nuclear gauge method) and collect sack samples for characterization of	Based on the results of this characterization identify 3 representative sample for water retention testing and perform the test content, density, gradation,	Analyze if conventional aspahlt system is sufficent to eliminate the need for Petromat pavement system outside the Dial area (Subtitle D cover)
		nd tests to determine subgrade modulus nd compressibility for slab-on-grade	value, maximum dry density and optimum moisture content, and compressibility tests and recompact selected collected soil to proposed design specifications (93% of maximum dry density at 110% of optimum moisture content) and perform consolidation tests on recompacted material	vegetative layer material at approximately 0.5-foot and 1.5-foot depth. Collect a total of 38 sack samples.  Perform 8 field plate load tests 1.5 feet below the ground surface. All plate load tests will be	and plasticity.  Perform 7 compressibility tests on the samples collected at the lower elevations. Perform 3 R-value tests on samples with the highest plasticity.  Perform 3 - 5 maximum dry density tests on characteristic sack samples.	Utilize the obtained data in pavement and slab-on-grade design
Retaining wall a	-	esigri	the subgrade materials including the foundation layer below the liner.	performed at the location of hand-auger boring.	None	
Northern Retaining Wall native materials	ment is located entirely on terials		Collect samples along the length of the wall alignment and in the backcut area and research historical and as-built information about the dike. Identify the kind and extent of refuse, man-made, and native materials. Perform conventional	Historical/as built information survey for the perimeter slope dike.  Perform topographic survey along the northern site boundary (by others).	Determine in situ mainture content density gradation plantisity compressibility	Prepare recommendations for foundation design, lateral pressures
long CMU retaining wall along the school property boundary)  It is expected the wall will extend the face of the wall wall extend the wall extend the wall extend the wall wall extend the w	xtend up to 9 feet behind to the wall and the backcut approximately at		geotechnical laboratory testing.  Topographic survey along the northern site boundary is required.	Excavate 6 borings using truck- or track- mounted hollow-stem drill rig along the toe of the wall alignment and approximately 6 borings on top of the slope behind the wall. Collect California Modified ring samples at 2- to 5- foot intervals and at least 20 feet into the native materials. Anticipate total boring depths of about 30 feet at the toe of the wall and 45 feet for borings drilled on top of the dike. Anticipate a total of about 8 to 15 samples per boring.	Determine in situ moisture content, density, gradation, plasticity, compressibility, and shear strength parameters.	on the retaining wall, sesimic design, and backcut slope stability.
(6 feet high 200 feet long CMU	for cement is located entirely on the	ompressibility and bearing capacity of	Collect samples along the length of the wall alignment and in the backcut area. Identify the kind and extent of refuse, man-made, and native materials. Perfom conventional geotechnical laboratory testing.	Excavate 2 borings using truck- and/or track- mounted hollow-stem drill rig along the wall alignment. Collect California Modified ring samples at 2- to 5- foot intervals and at least 15 feet into the native materials. Anticipate total boring depths of about 15 feet. Anticipate a total of about 5 samples per boring.	Determine in situ moisture content, density, gradation, plasticity, compressibility, and shear strength parameters.	Prepare recommendations for foundation design, lateral pressures on the retaining wall, and backcut slope stability.
Western Retaining Wall (CMU retaining wall along the west property boundary, 1.5 to 8 feet high, approximately 800 feet long)  Southwest portic located mostly of	ostly outside the refuse AC overlay cover the Lt portion of the wall is ostly on refuse but also on terials on Subtitle D-	valuate depth, condition, uniformity, and ompressibility and bearing capacity of ne vegetative layer, foundation layer, and nderlying foundation subgrade materials and ative soil	In the areas above the refuse collect samples of the vegetative layer and perform basic geotechnical laboratory testing.  In the areas above native materials collect samples of the cover and penetrate about 10 feet into the native materials and perform basic geotechnical laboratory testing.	In the areas above the refuse excavate 6 borings to the GCL liner using hand-auger at no more than 200-foot intervals along the wall alignment and perform a field moisture and field density tests (snad cone or nuclear gauge method) and collect sack samples for characterization of vegetative layer material at approximately 0.5-foot and 1.5-foot depth. Collect a total of 12 sack samples.  In the northwest where no refuse is identified in the as-built plans where the wall will be 7 to 8 feet high excavate 2 truck-mounted hollow stem borings through the existing 2" AC overlay to a depth of at least 8 feet. Repair the AC overlay cover per work plan.  In the southwest corner where no refuse is identified in the as-built plans where the wall will be 1.5 to 2.5 feet high excavate 1 truck-mounted hollow stem boring through the existing Subtitle-C cover to a depth of at least 8 feet. Repair the cover per workplan.  In all hollow stem borings collect relatively undisturbed California Modified sampler ring samples of native materials at approximately 2-foot vertical intervals starting about 1 foot below the existing grade AND	Determine in situ moisture content, density, and compressibility.	Prepare recommendations for retaining wall foundation design and preparation of the subgrade.
			In areas above the refuse use the plate load test above the GCL layer to obtain compression characteristics of the subgrade materials including the foundation layer below the liner.	Perform about 4 field plate load tests 1.5 feet below the ground surface along the wall alignment. All plate load tests will be performed at the location of hand-auger boring.	None	
The easement is above refuse an soils. The existing engineered control of the con		etermine <b>subgrade modulus</b> and	Core the existing concrete cover <u>above the anticipated native soils</u> and determine subgrade modulus and compressibility for slab-on-grade/concrete pavement design.	At 1 location above the native soils core the existing concrete cover and advance 1 truck-mounted hollow stem auger boring to a depth of about 8 feet and collect about 3 relatively undisturbed California Modified sampler ring samples for characterization of the native soils starting at a depth of approximately 1 foot at approximately 2-foot vertical intervals and about 2 composite sack samples.	Determine in situ moisture content, density, gradation, and plasticity and perform 2 compressibility tests on the collected samples.	Utilize the obtained data for slab-on-
support intender the design it is prepare the sub surficial recomp observed subgri			Sawcut the existing concrete cover <u>above the anticipated refuse</u> and perform field plate load tests to determine subgrade modulus and compressibility for slab-ongrade/concrete pavement design.	At 1 location above the refuse sawcut the exisiting concre cover and perform plate load test on the exposed surface.		grade/pavement design
Southern Retaining Wall (1.5 to 2.5 feet high, approximately	ment is located mostly on vered by Subtitle D-	valuate depth, condition, and ompressibility and bearing capacity of ne vegetative layer, foundation layer, and nderlying foundation subgrade materials and	Collect samples of the vegetative layer along the length of the wall alignment. Excavate shallow borings and sample the vegetative cover material Perform basic geotechnical laboratory testing.	Excavate 4 borings using hand-auger at no more than 200-foot boring intervals along the toe of the wall alignment and perform a field moisture and field density tests (sand cone or nuclear gauge method) and collect sack samples for characterization of vegetative layer material at approximately 0.5-foot and 1.5-foot depth. Collect a total of 8 sack samples.  AND	Determine in situ moisture content, density, and compressibility.	Prepare recommendations for retaining wall foundation design and preparation of the subgrade.
equivalent cover	t cover		Perform plate load test above the GCL layer to obtain compression characteristics of the subgrade materials including the foundation layer below the liner.	Perform about 4 field plate load tests at 1.5 feet below the ground surface along the wall toe.	None	

			TABLE 3-1 - Geot	echnical Investigation Matrix		
				d Landfill Redevelopment		
				Investigation Activi	ity	
Development Element	Design Consideration	Needed Parameters	How to Obtain Needed Parameters	Field Investigation (Repair any disturbance of the cover per workplan; additional specific repair requirements are stated in the matrix)	Lab Testing	Engineering Processing of Data
600 feet long, CMU retaining wall	Wall alignment is located on refuse	Evaluate depth, condition, uniformity, and compressibility and bearing capacity of the vegetative layer, foundation layer, and underlying foundation subgrade materials and native soil	In the areas above the refuse collect samples of the vegetative layer and perform basic geotechnical laboratory testing.  In the areas above native materials collect samples of the cover and penetrate about 10 feet into the native materials and perform basic geotechnical laboratory testing.	Thoring through the existing Subtitle-C cover to a depth of at least 8 teet and collect about 3 relatively.	Determine in situ moisture content, density, and compressibility.	Prepare recommendations for retaining wall foundation design and preparation of the subgrade.
			<u>In areas above the refuse</u> use the plate load test above the GCL layer to obtain compression characteristics of the subgrade materials including the foundation layer below the liner.	Perform 2 field plate load tests 1.5 feet below the ground surface along the wall alignment. All plate load tests will be performed at the location of hand-auger boring.	None	
PROVISIONAL	Foundation design	Native/fill soil conditions in the foundation subgrade to determine <i>compressibility</i> and	Collect samples within the footprint of the building. Evaluate the conditon of native	Excavate 4 borings using truck-mounted drill rig in the corners and center of the proposed building to	Determine in situ moisture content, density, gradation, plasticity, compressibility,	Prepare recommendations for building
On-site Building	Located on native materials in the northeast corner	bearing capacity of the native subgrade materials	materials. Perfom conventional geotechnical laboratory testing.	depths of 20 to 40 feet. Collect California Modified ring samples at 2- to 5- foot intervals. Anticipate a total of about 8 to 13 samples per boring.	shear strength parameters, and soil corrosion potential.	structural and civil design.
— PROVISIONAL — SUBJECT TO SPECIFIC WORK PLAN  Light Towers / Poles (size, locations, and number not yet determined)	Foundation design	assumed that the ligh posts will be all located along the perimeter of the site and outside the refuse areas	SPECIFIC WORK PLAN WILL BE SUBMITTED UNDER A SEPARATE COVER PENDING DEVELOPER/CITY DECISION  For tall (>-30 feet) light towers collect samples at the tower locations. Identify the kind and extent of refuse, man-made, and native materials. Perfom basic geotechnical laboratory testing.  For short light poles (<-30 feet) no special investigation may be necessary and the subgrade conditions may be extrapolated from available data.	At tower locations excavate 1 boring per structure using truck-mounted drill rig to depths of 20 to 40 feet. Collect California Modified ring samples at 2- to 5- foot intervals. Anticipate a total of about 5 to 10 samples per boring.  Assume that no investigation will be necessary at light pole locations.	Determine in situ moisture content, density, gradation, plasticity, compressibility, shear strength parameters, and soil corrosion potential.	Prepare recommendations for structural and civil design.

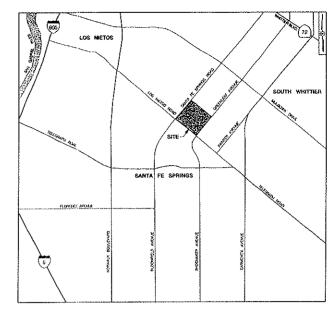
# **APPENDIX A**

# **As-built Plans for the Site Remedy**



# SOILS, SUBSURFACE **GAS AND GROUND WATER REMEDY**

WASTE DISPOSAL, INC. SUPERFUND SITE SANTA FE SPRINGS, CALIFORNIA



SITE LOCATION MAP

# CERTIFICATION

FINAL DESIGN REPORT (REVISION 1.0) SOILS, SUBSURFACE GAS, AND GROUND WATER REMEDIAL DESIGN

These Drawings for the Waste Disposal, Inc., Superfund Site were prepared by TRC on behalf of the Waste Disposal, Inc., Group (WDIG) in a manner consistent with the level of care and skill ordinarily exercised by professional engineers. Those Drawings were prepared under the technical direction of the undersigned, California Registered Grid Engineers.

Executed at Irvine, California this \_\_\_\_ a day of March 2003.





#### GENERAL NOTES 1. THE WORK SHOWN BY THIS DOCUMENT IS FOR THE WASTE DISPOSAL INC. GROUP, HEREAFTER REFERRED TO AS THE WORK

- THE PLANS AND OTHER DOCUMENTS (a.g., SPECIFICATIONS) SHALL GOVERN THE WORK AND SHALL BE CONSIDERED
  COMPLINENTAMY, ANYTHING FOUND IN THE PLANS AND NOT IN ANOTHER DOCUMENT OR FOUND IN ANOTHER DOCUMENT
  AND NOT IN THE PLANS SHALL BE CONSIDERED TO GE IN BOTH. IF THERE ARE DISCREPENCIES BETWEEN PLANS AND OTHER
  COMPLINENTAMY DOCUMENTS THE CONTRACTION IS PREQUIRED TO ASK THE WIND SITE REPRESENTATIVE FIGH CLARIFICATION.
- CONTRACTOR SIMLE, ON DISCOVERING ANY ERROR OR OMISSION IN THE PLANS, IMMEDIATELY BRING IT TO THE ATTENTION OF THE WORD SITE REPRESENTATIVE.

- 7. CONTRACTOR SHALL KEEP A COPY OF THE PLANS AND OTHER DOCUMENTS AT THE WORK SITE.
- CONTRACTOR SIMIL ASCERTAIN THE EXISTENCE OF ANY CONDITIONS AFFECTING THE COST OF THE WORK WHICH WOULD HAVE BEEN DISCLOSED BY REASONABLE EXAMINATION OF THE SITE.
- EXISTING IMPROVEMENTS VISIBLE AT THE JOB SITE, FOR WHICH NO SPECIFIC DISPOSITION IS MADE ON THE PLANS, BUT WHICH COULD RESSONABLY BE ASSUMED TO INTERFERE WITH SATISFACTIONY COMPLETION OF THE WORK, SHALL BE BROOMED IT OT THE THEN HOLD FIT WORS STEE REPRESENTATIVE.
- SOIL, MATERIAL REQUIRED FOR THE WORK SHALL BE STOCKPILED AT LOCATIONS SPECIFIED IN THESE PLANS OR AS DESIGNATED BY THE WORK SITE REPRESENTATIVE.

- 14. ALL IN-FIELD MODIFICATIONS REQUIRE APPROVAL BY THE WORD SITE REPRESENTATIVE PRIOR TO IMPLEMENTATION

- 17. BORING LOGS ARE AVAILABLE FOR REVIEW BY CONTRACTOR UPON REQUEST. SUBSURFACE DATA AND INFORMATION

PREPARED FOR: WASTE DISPOSAL, INC. GROUP (WDIG)

### PREPARED BY: TRC

21 TECHNOLOGY DRIVE **IRVINE, CALIFORNIA 92618** (949) 727-9336

		INDEX OF DRAWINGS
SHEET NO.	FILE NO.	TIBLE
1 *	E-30747-SGOX-1	TRUE, INDEX, LEGENO AND GENERAL HOYES
2	E-30747-SG0C	EXISTING TOPOGIMPHY - PRE-REMEDIAL CONSTRUCTION
3	E-30747-SG008	EXISTING SURFACE COVER - PRE-RUMEDIAL CONSTRUCTION
4	E-30747-SG0%	BORING LOCATIONS - PRE-REHEGIAL CONSTRUCTION
5	E-30747-SG0:4	ISOPACH OF FILL THICKNESS ABOVE WASTE (INCLUDING ANOHOLIES) - PRE-REHEDIAL CONSTRU
6	E-30747-SG0/S	ISOPACH OF FILL THICKNESS ABOVE WASTE (INTERPRETED) - PRE-REMEDIAL CONSTRUCTION
7*	E-30747-\$G0:9	SURFACE GRADING PLAN (TOP OF COVER)
8	E-30747-SG076	EXISTING EARTH COVER THICKNESS - PRE-REMEDIAL COUST RUCT YON
9*	C-30747-SG023	COVER TYPE PLAN, PAVEMENT REHAB PLAN
10*		SECTIONS AND DETAILS
\$1#-		SOIL GAS EXTRACTION, VENTING AND TREATMENT SYSTEM SECTIONS AND DETAILS
12 *	E-30747-SG014	LOCATIONS OF LEACHATE COLLECTION WELLS, BIOVENT WELLS, VAPOR MONITORING WELLS.
		GROUND WATER MONITORING WELLS AND SETTLEMENT MONUMENTS
13 *	E-30747-SG013	BIOVENT WELL, VAPOR MONITORING WELL AND GROUND WATER MONITORING WELL DETAILS
14 +	E-30747-SG0t6	LAYOSCAPING AND FENCING PLAN
15	E-30747-SG0:1	TYDROLOGY MAP 100 YEAR STORM - DESIGN
16 🔻	E-30747-SG002	CONSTRUCTION EROSION CONTROL PLAN
17*	E.23,234+2-5E1	ELECTRICAL SITE PLAN
48*	E-29011402-5(v)	ELECTRICAL SITE DETAILS
74*	E-29022402-56 . 13	AS-BUILT SUBGRADE TOPOGRAYAY

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### LEGEND

GEN	ERAL LINES
	PROPERTY BOUNDARY
	MAIN TOPIC OF DRAWING
	SUBTOPIC OF DRAWING
***************************************	CENTER LINE
	HIDDEN LINE
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		740	AGI TO LE CONCINCIE
	EXISTING SUIL COVER	AD\$	ADVANCED DRAINAGE SYSTEM
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	EXISTING CXNCRETE	BGS	BELOW GROUND SURFACE
	CONCRETE	Ф	CENTER LINE
	EXISTING ASSYMALT	CY	CUBIC YARD
	ENGINEERED ASPHALT COVER	DIA	DIAMETER
17772	EXISTING BULDING	DIM.	DIMENSION
	RCRA SUBTILE C - EQUIVALENT CAP	f:	EASTING
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	SOIL GAS NONCOMPLIANCE AREA	FG	FINISH GRADE
17/17/12	EXISTING GRADE	FIPT	FEMALE IRON PIPE THREAD
	DRAINAGE FOCK	A.	FLOW LINE
	BURIED WASTE	PM	PLOW METER
	AGGREGATI: BASE COURSE	ET	FEET
	RCRA SUBTINLE D - EQUIVALENT COVER	CD	CONSTRUCTION DEMOL

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1	ENGINEERED ASPHALT COVER					TI	TEMPERATURE INDICATOR
					KEY		

HANDWRITING ILLUSTRATES AS-BUILT REVISIONS

FILL PATTERNS

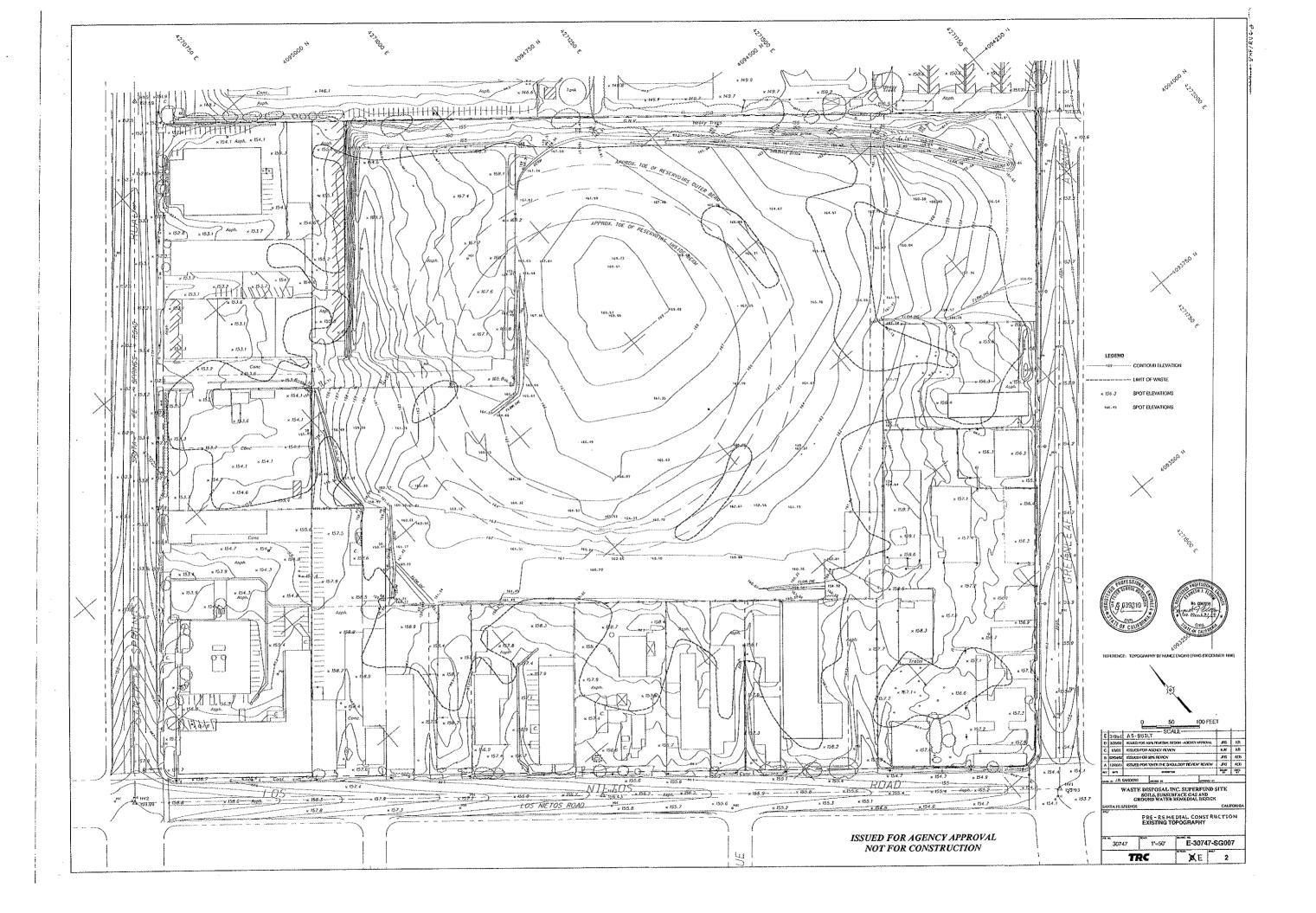


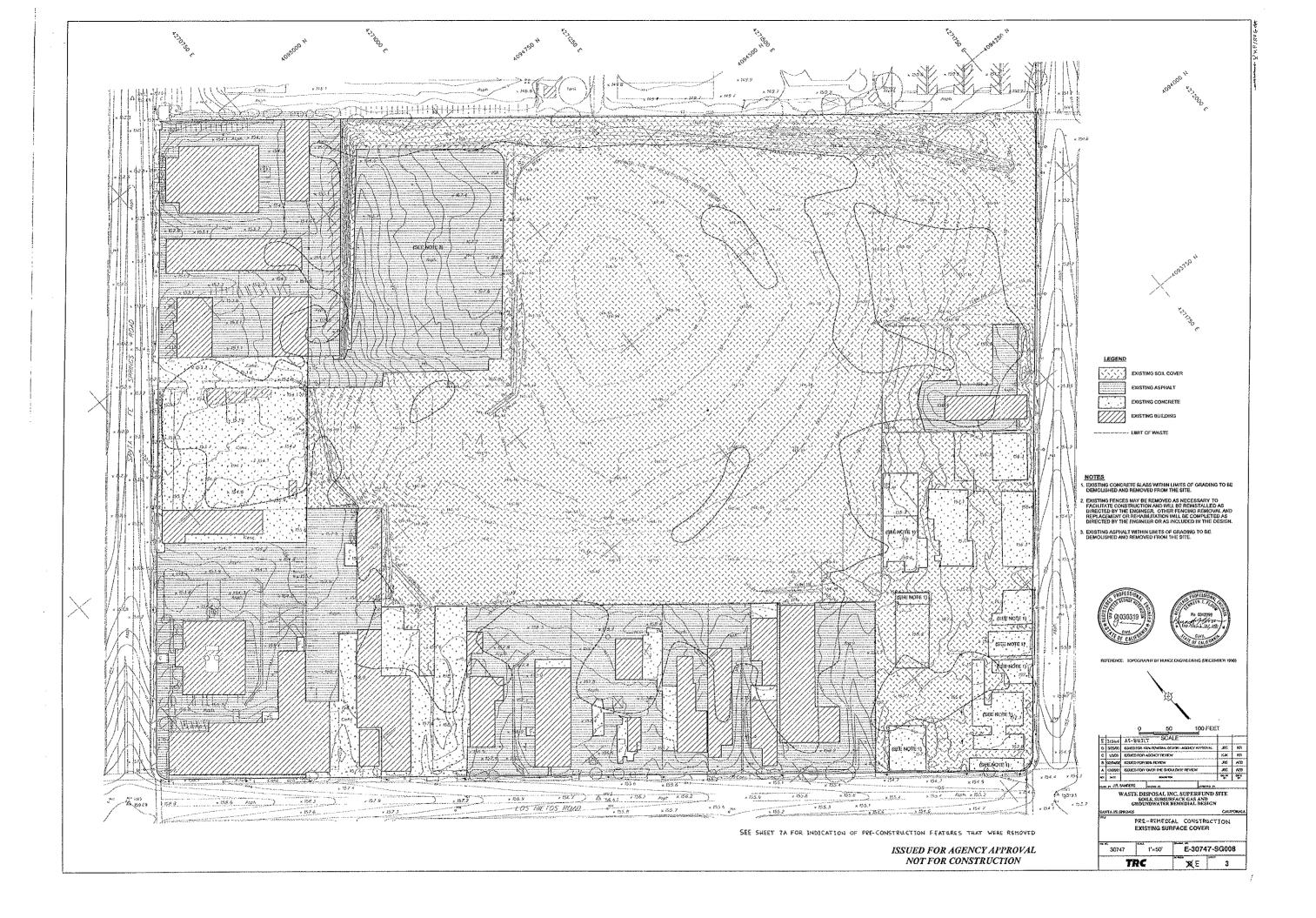
ABBREVIATIONS

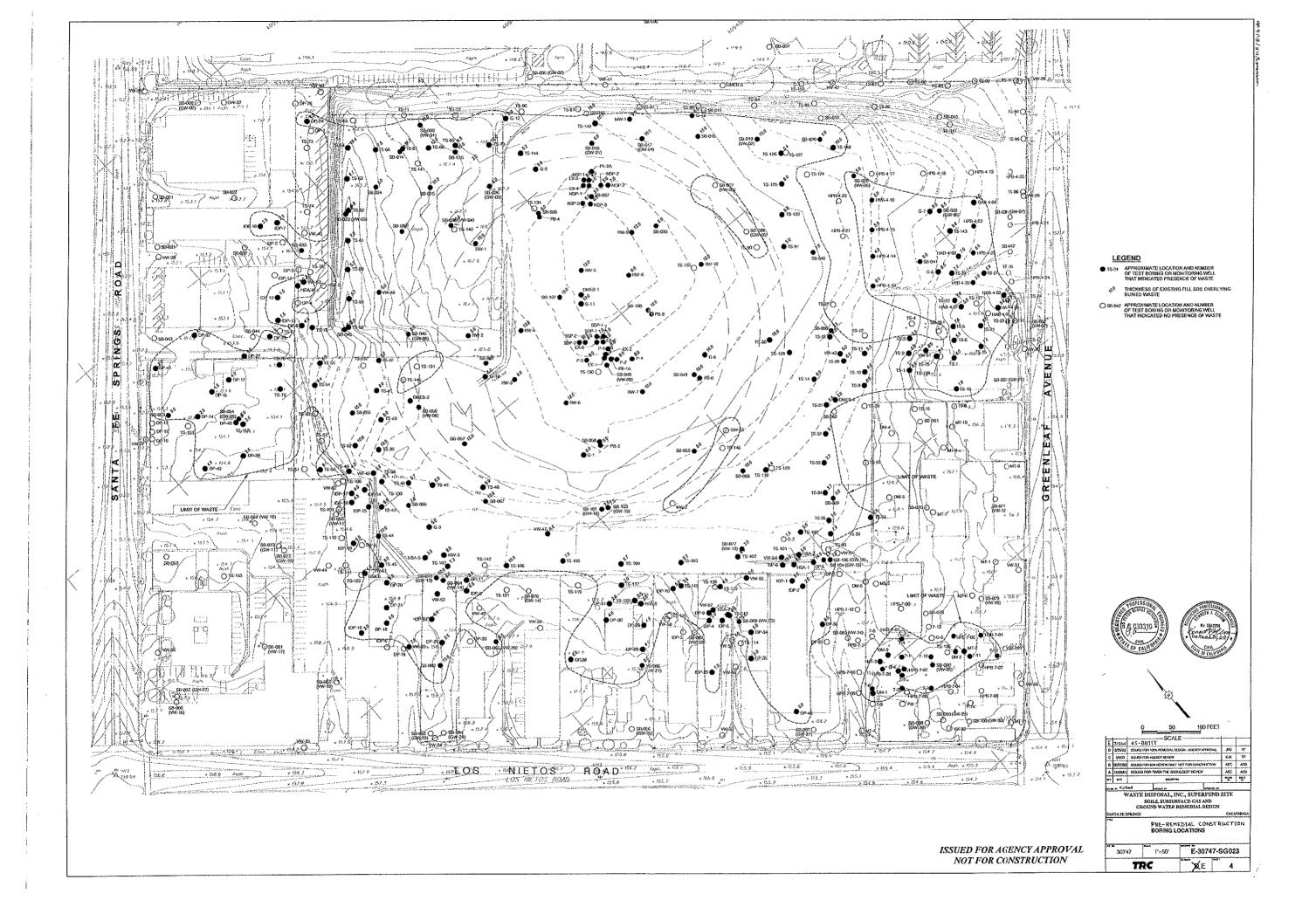
GRADE BREAK HIGH DENSITY POLYETHYLENE

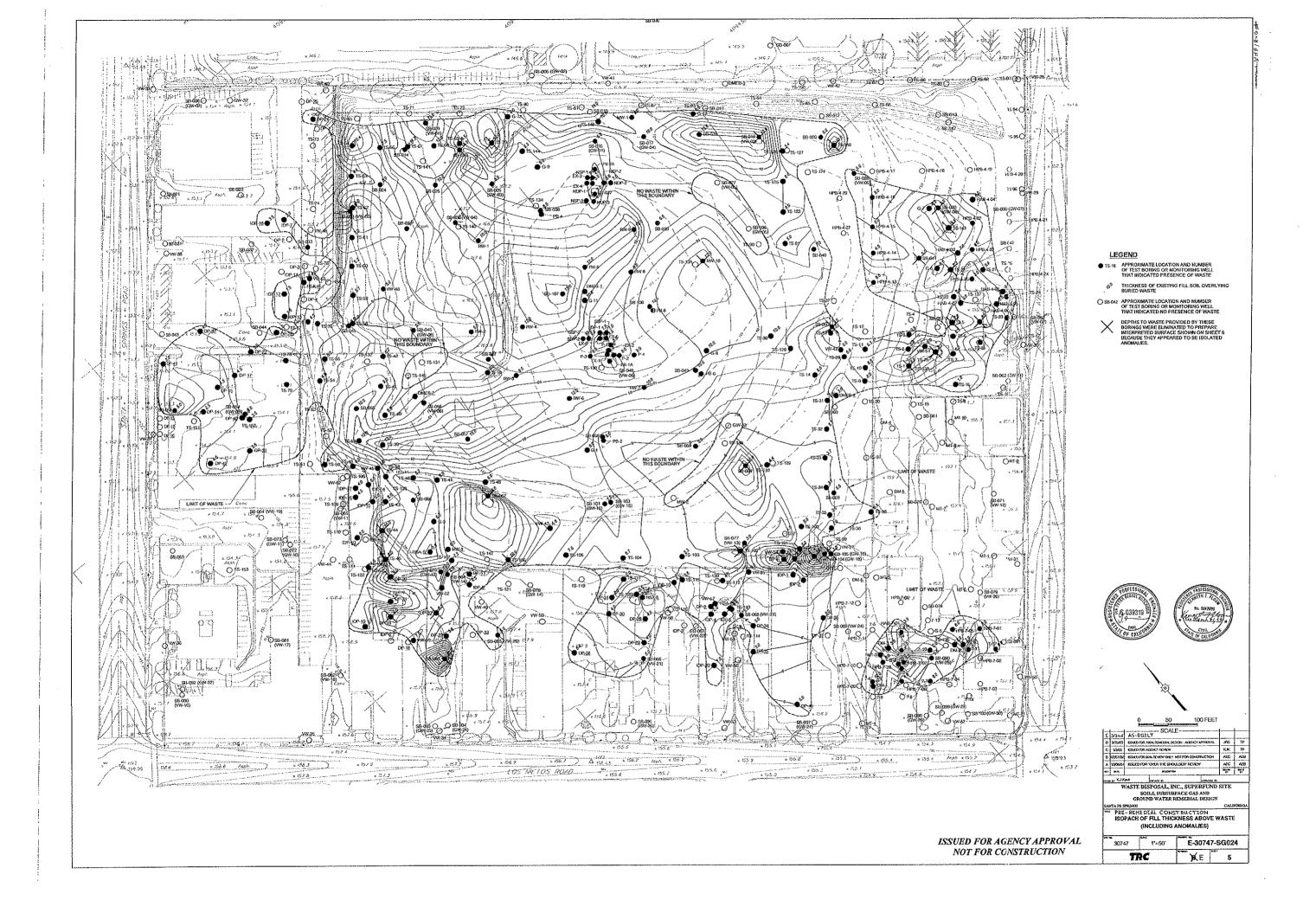
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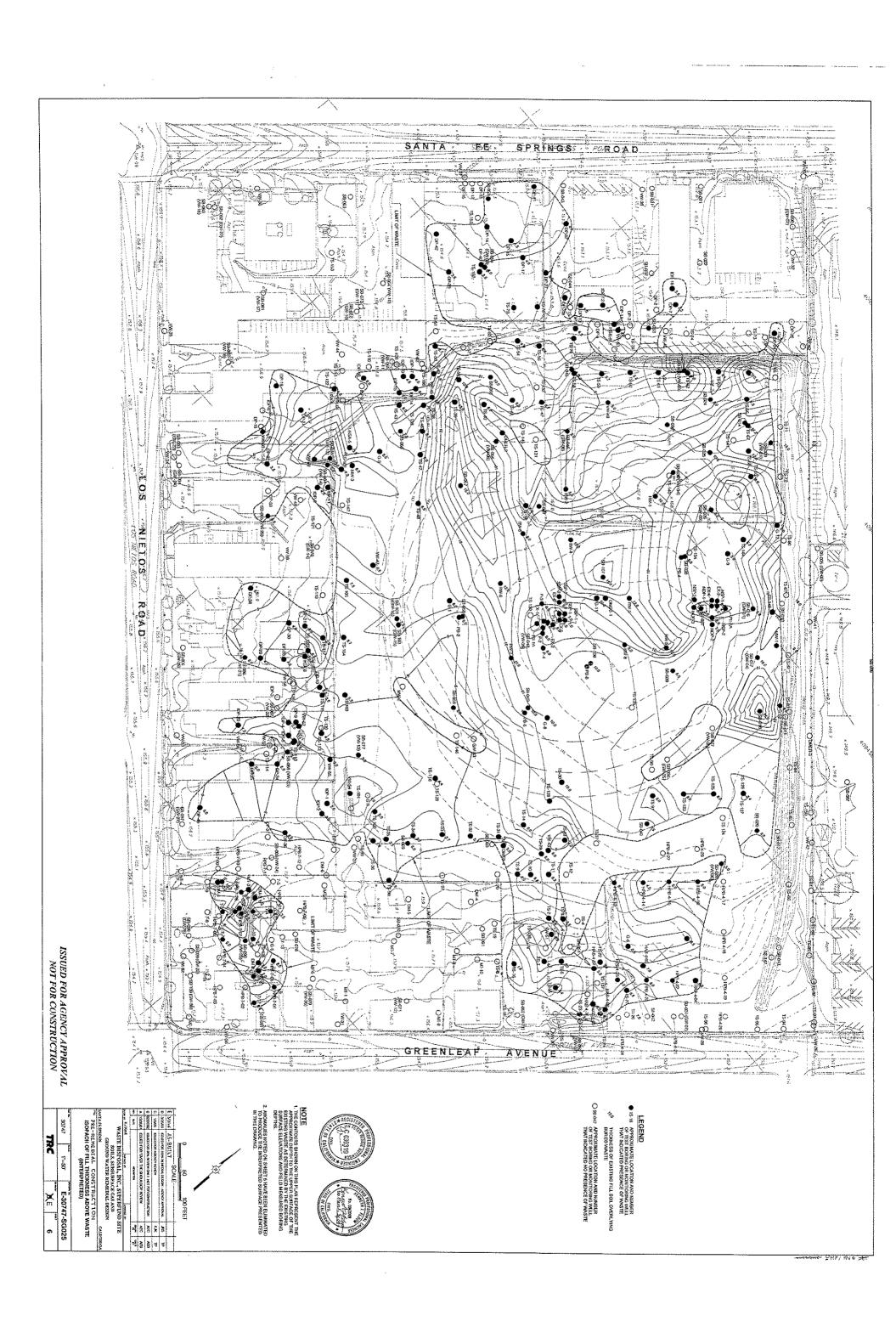
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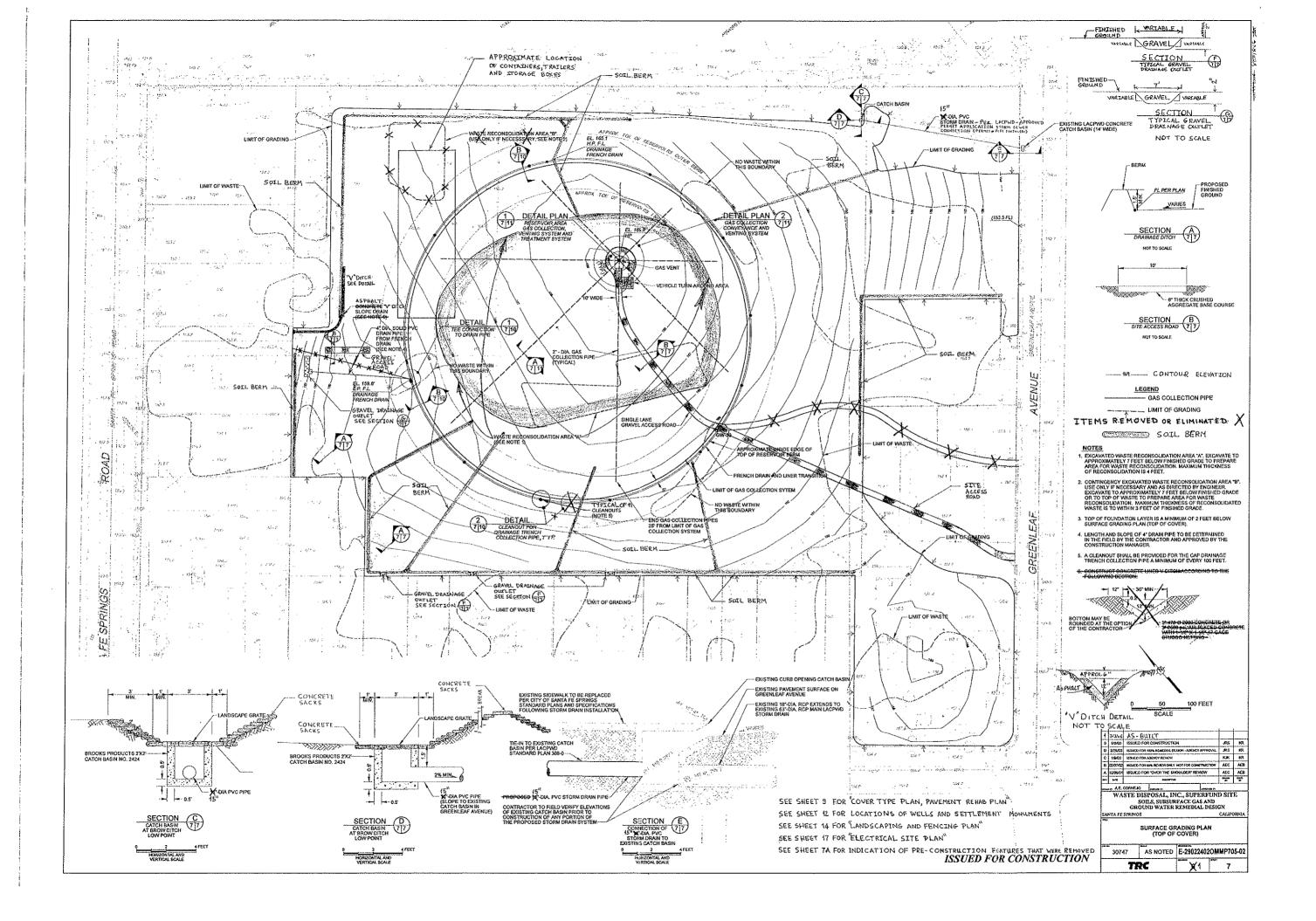


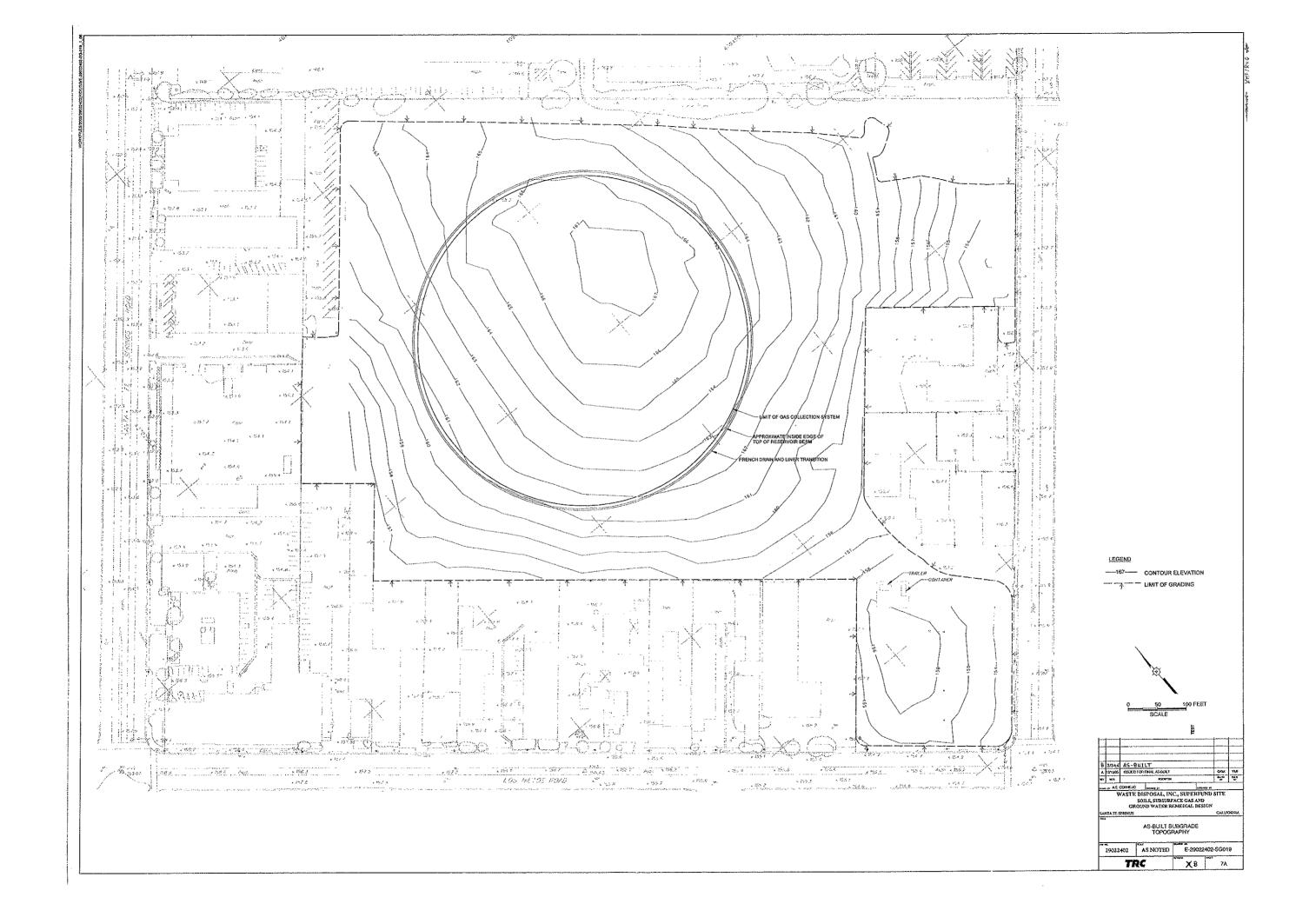


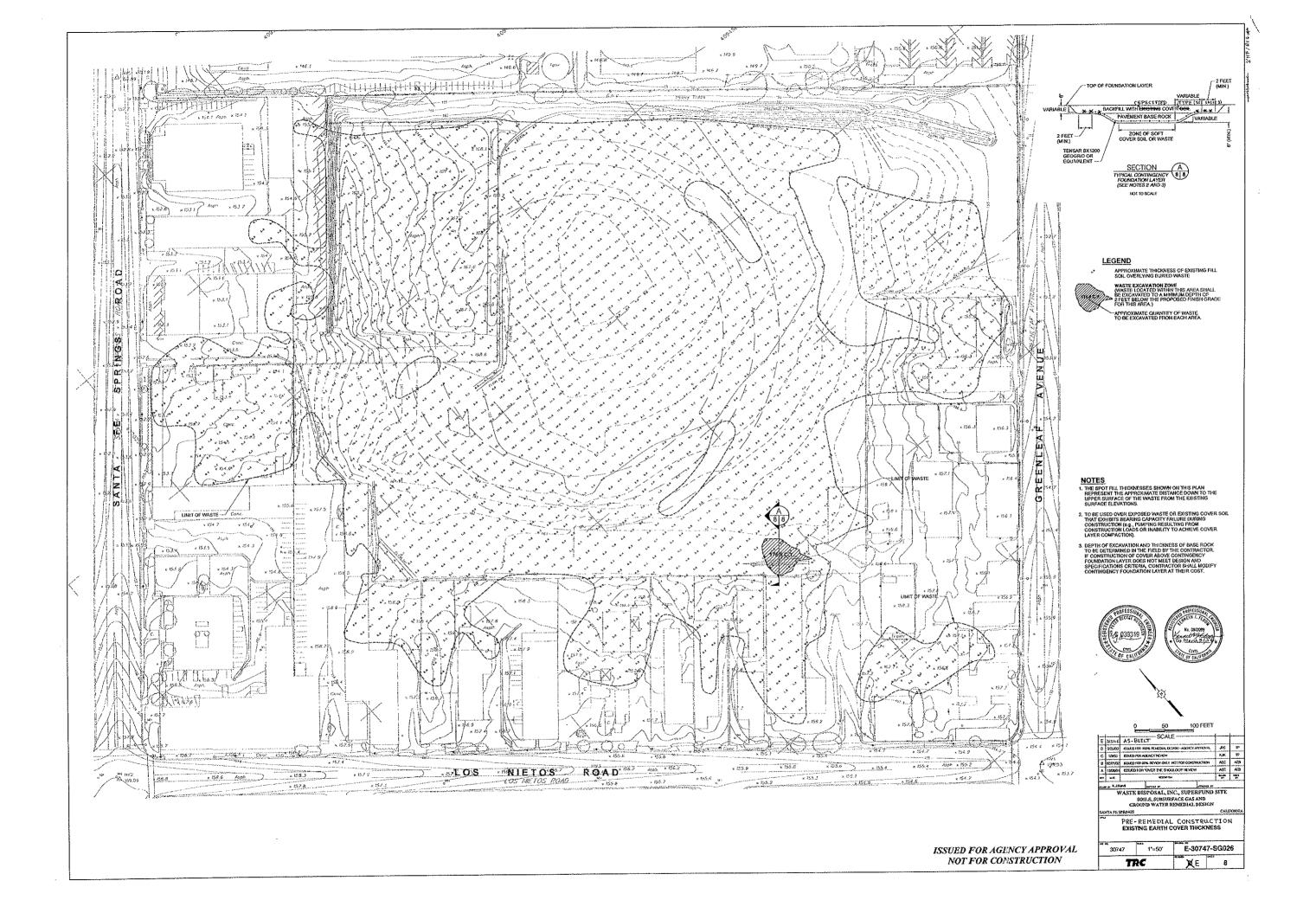


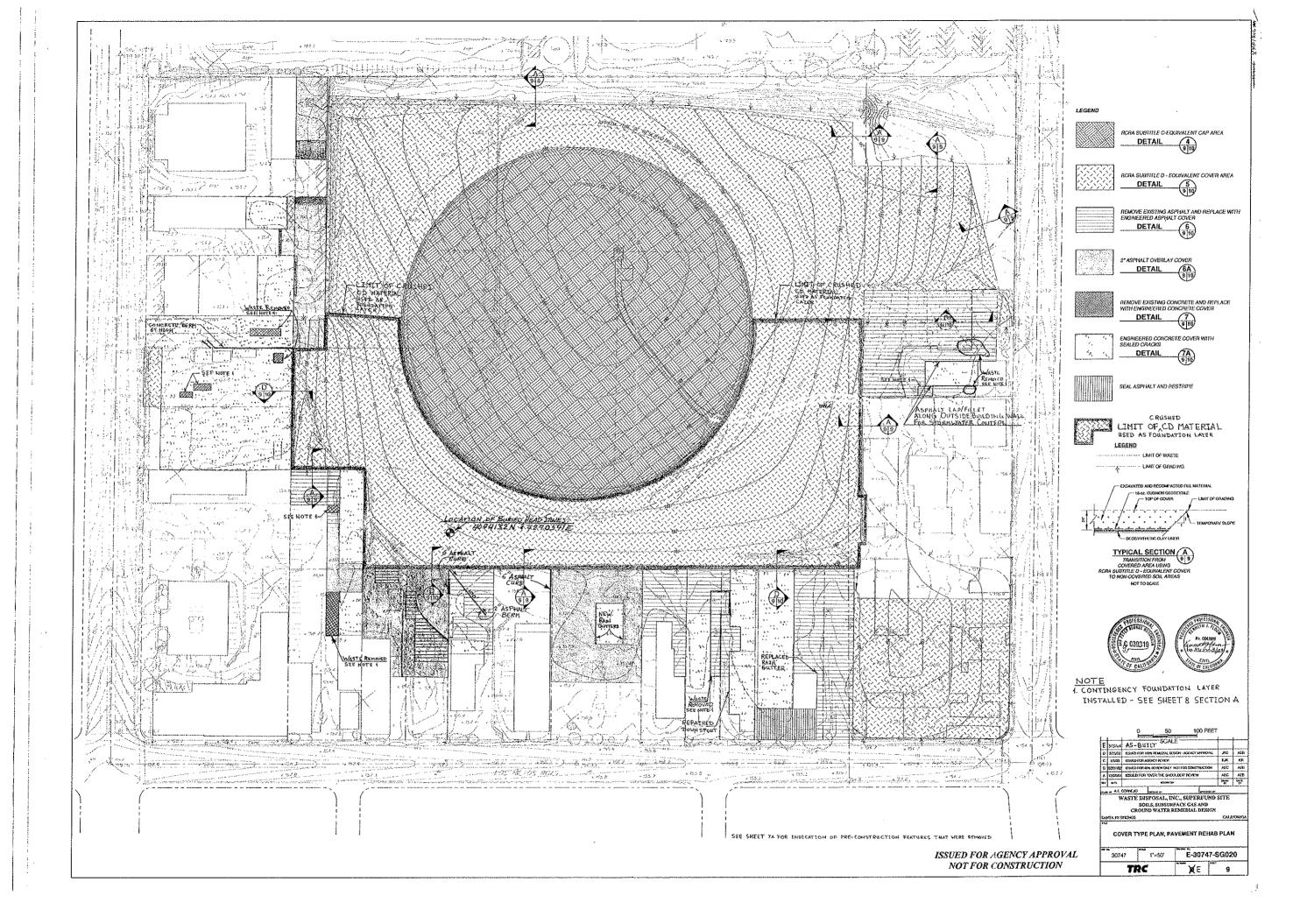


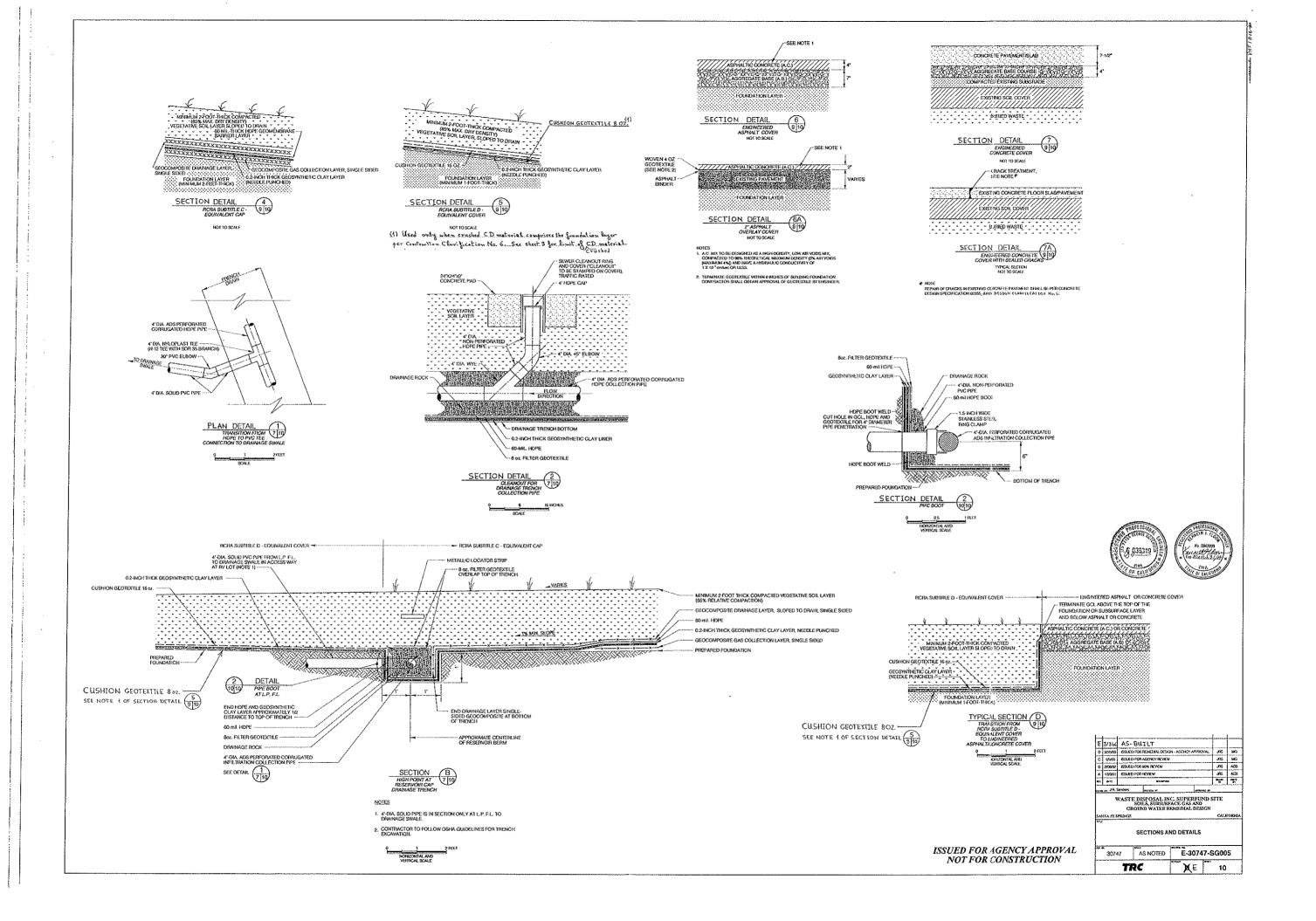


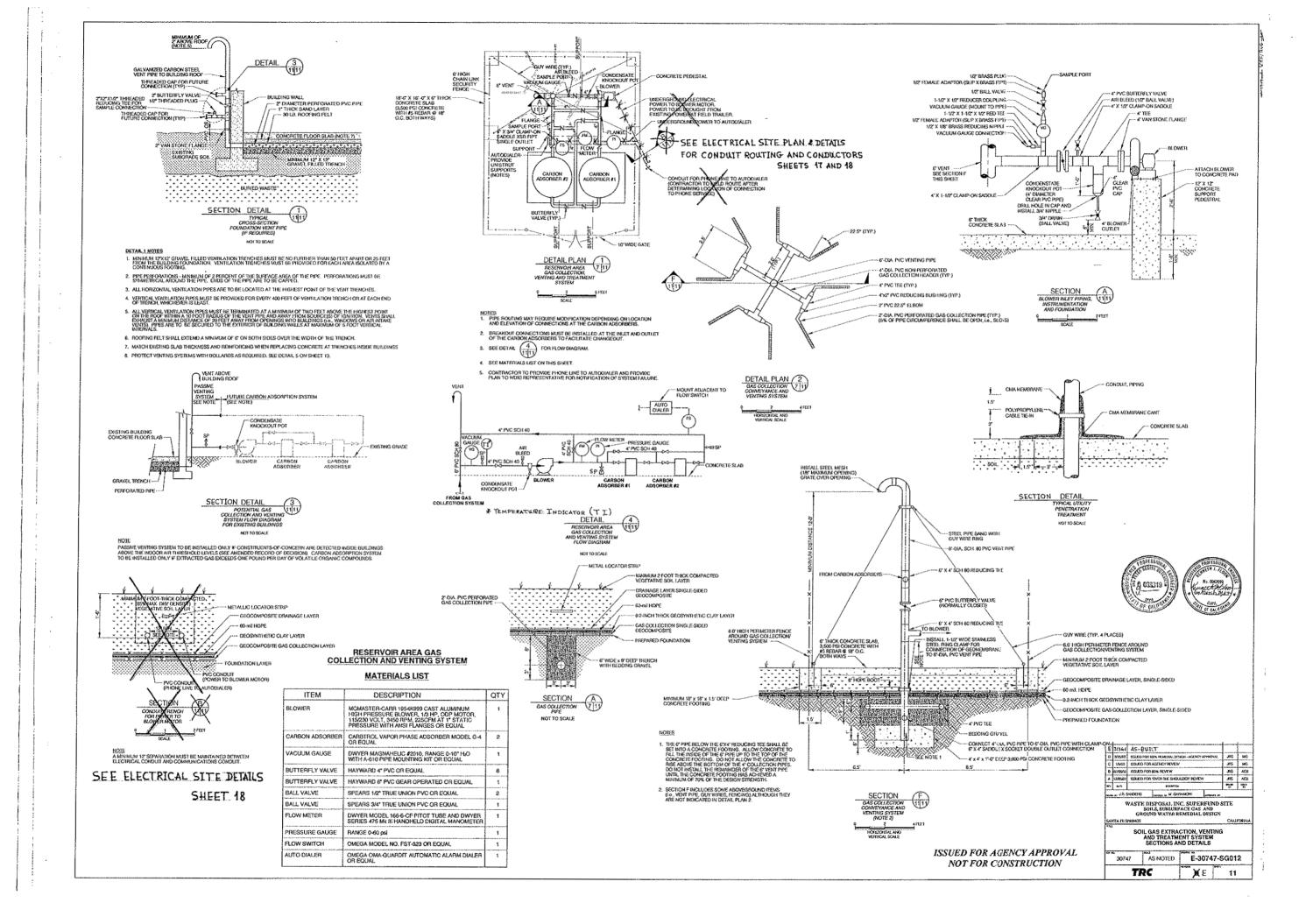


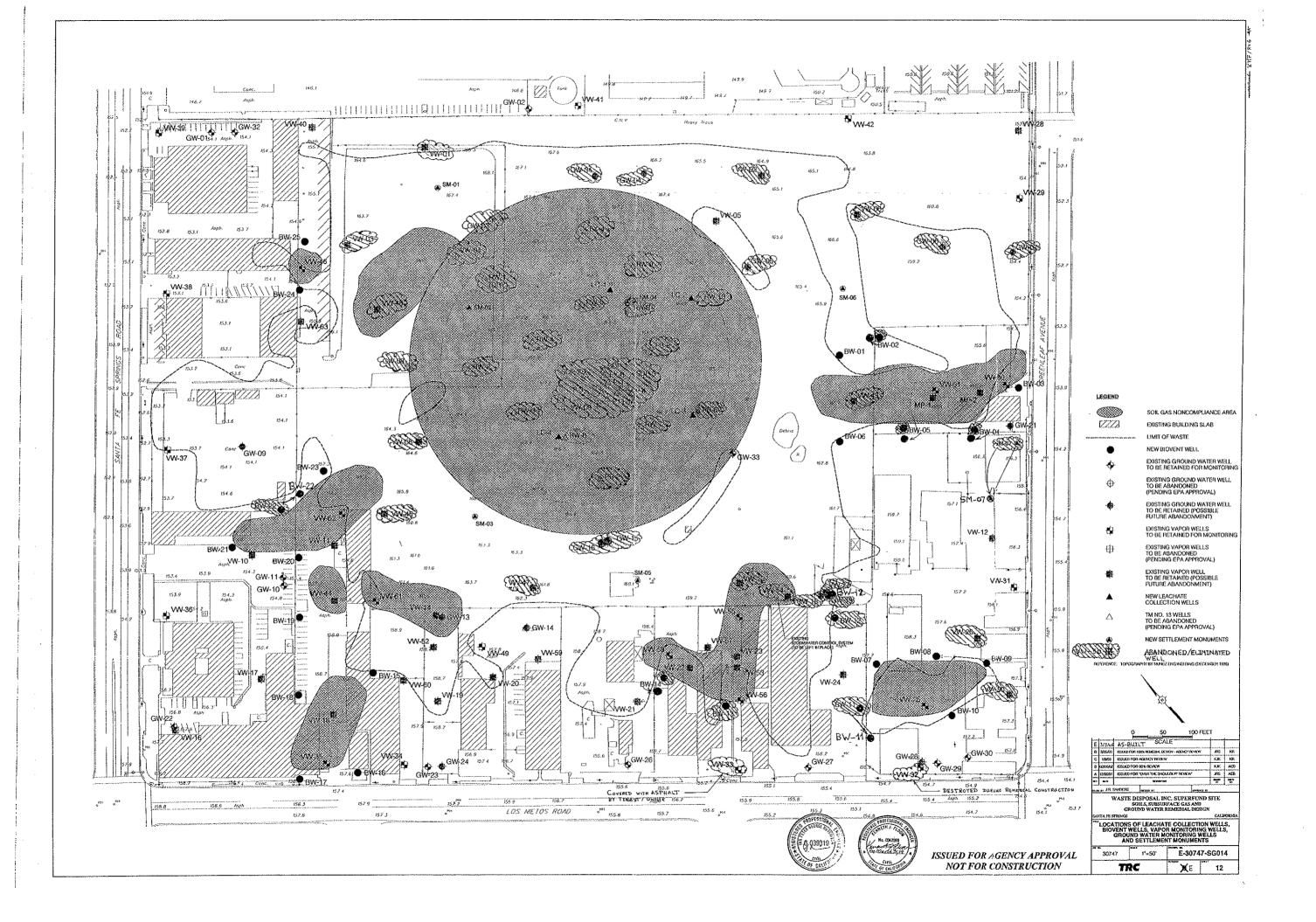


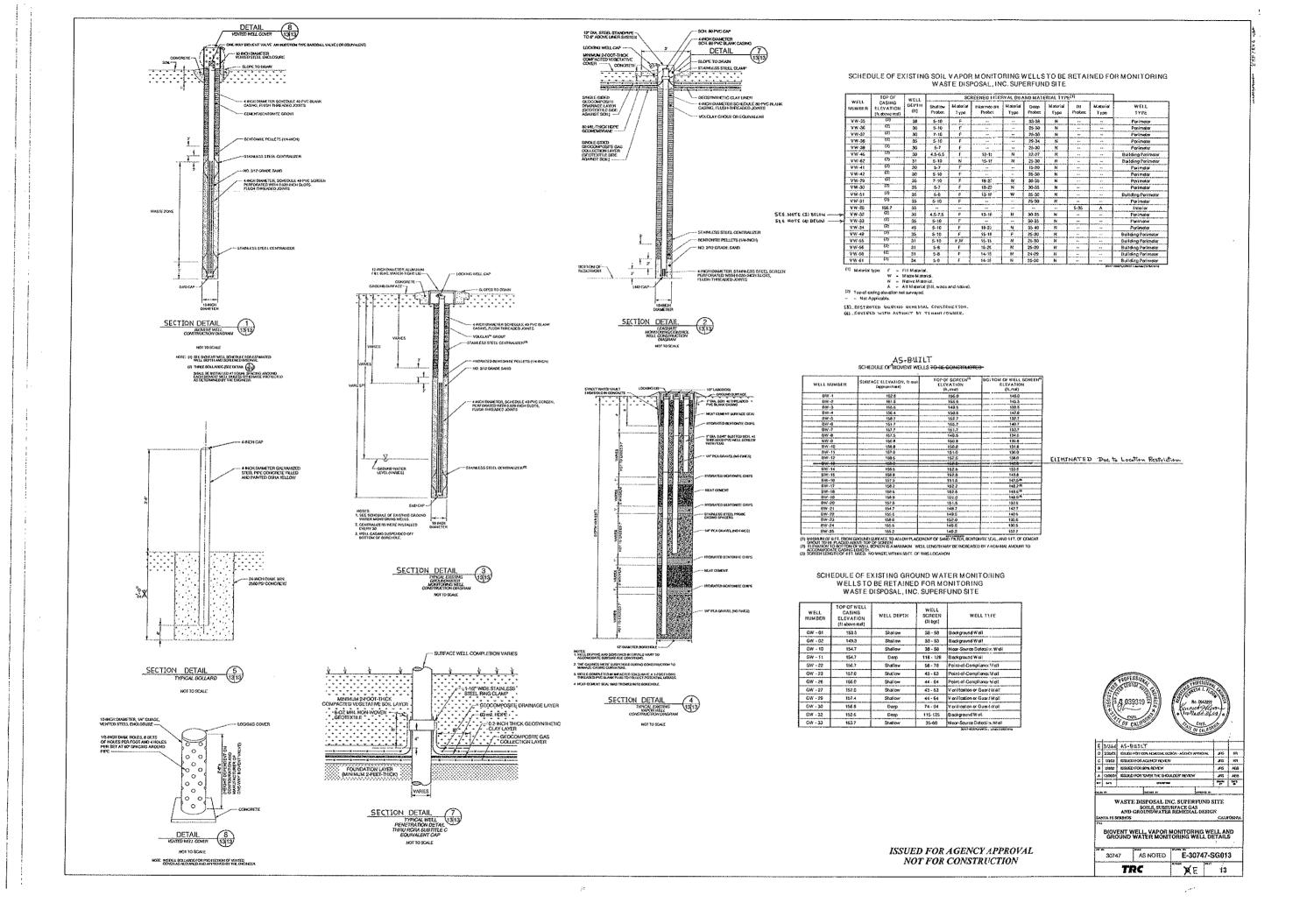


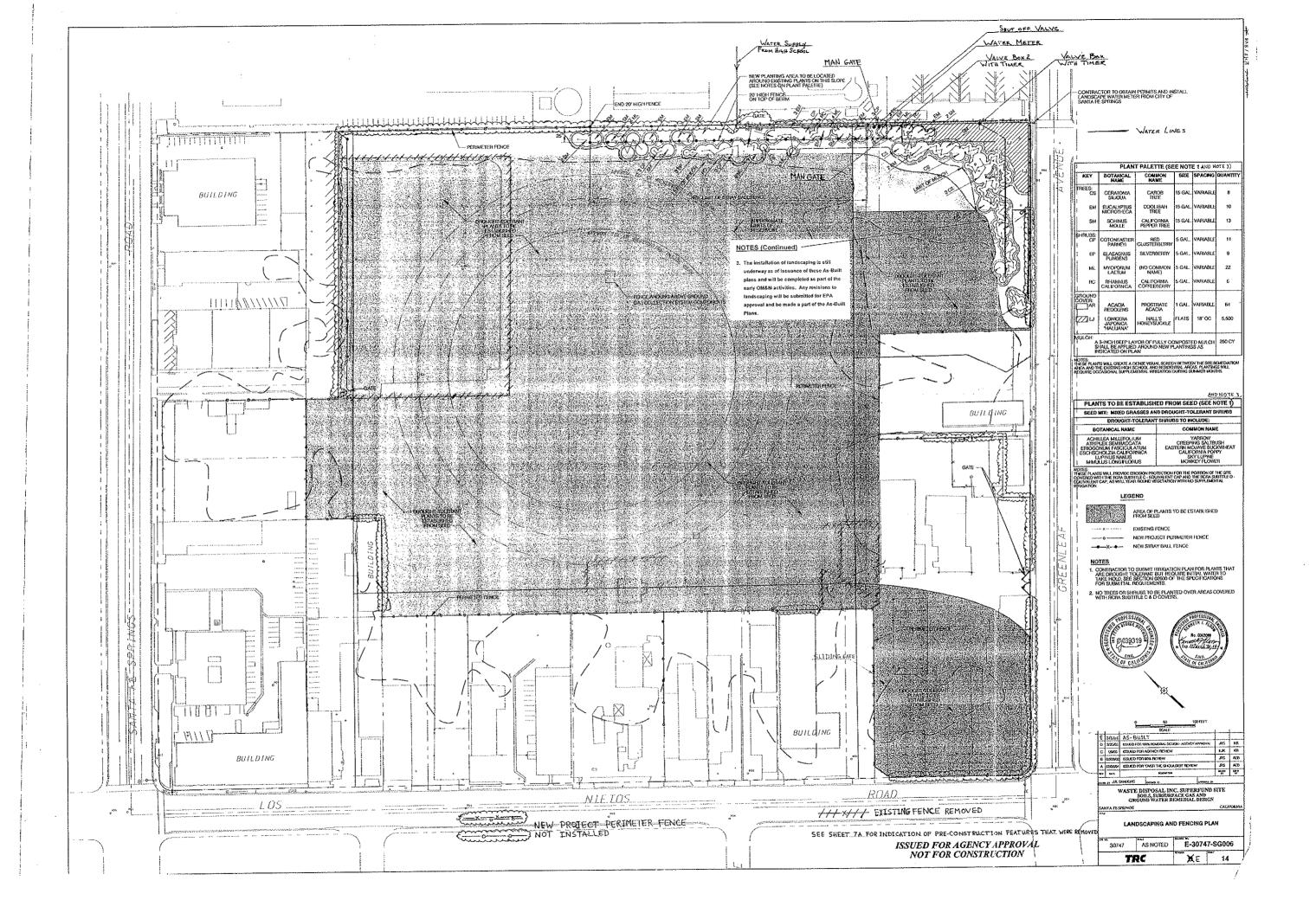


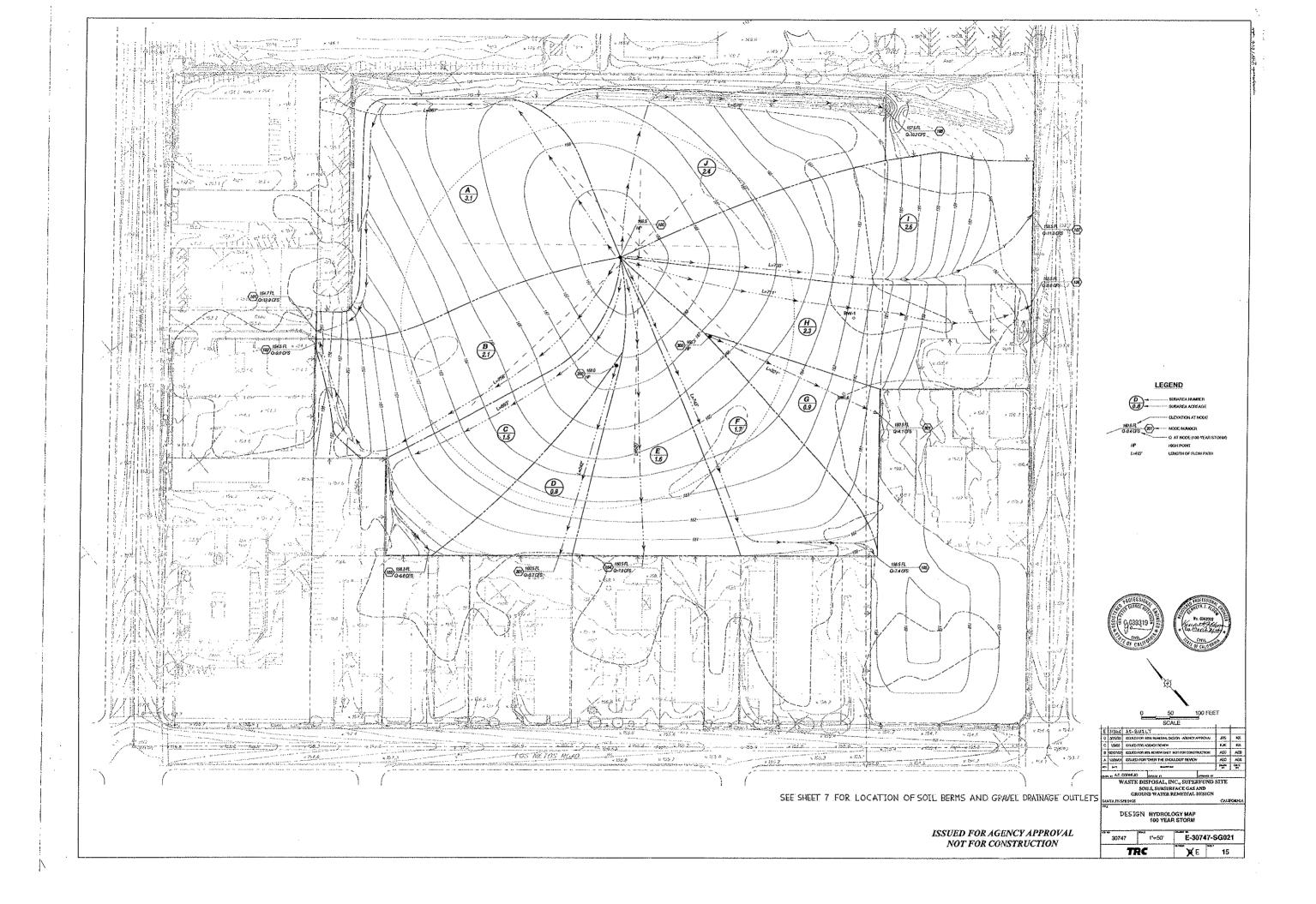


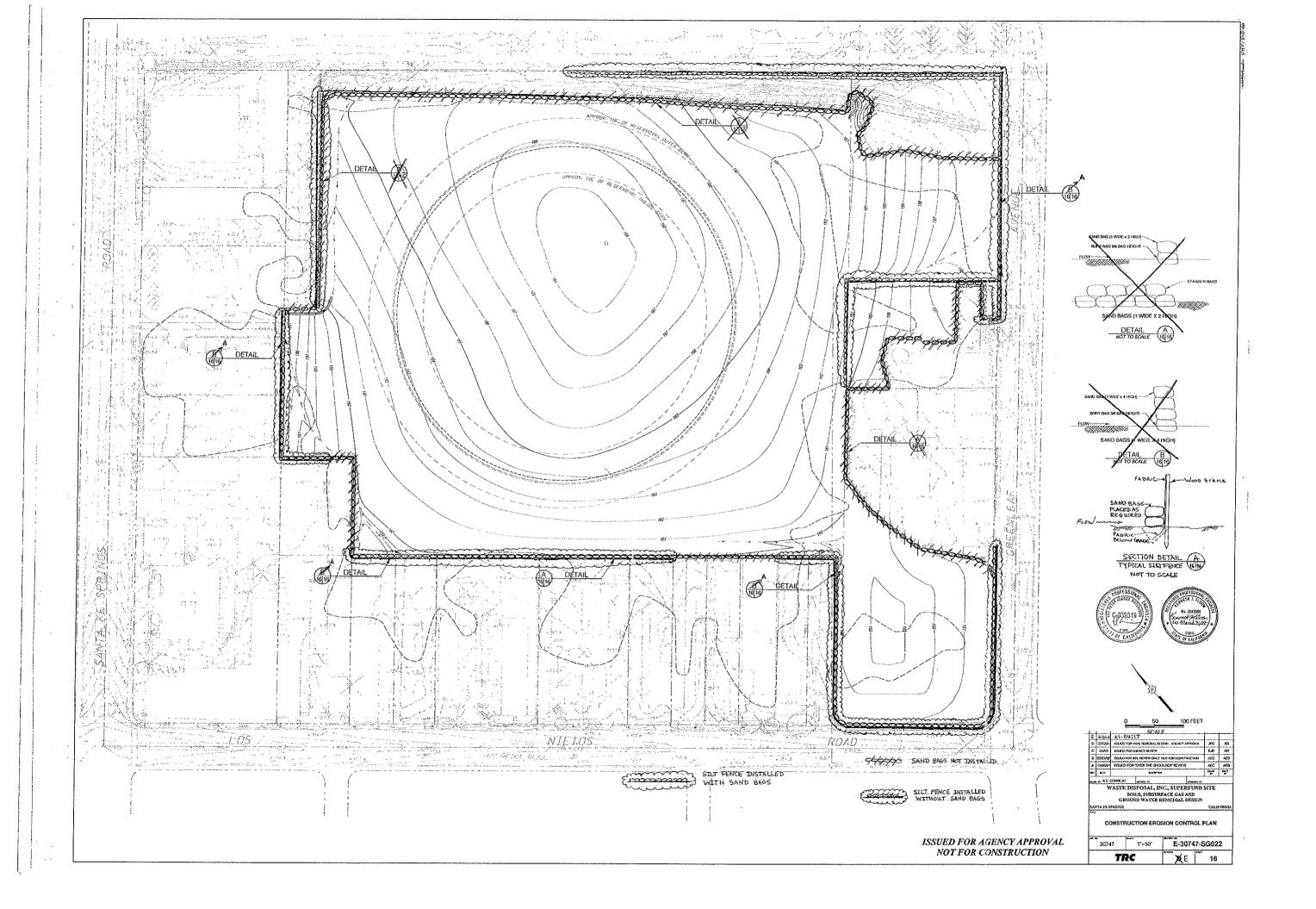


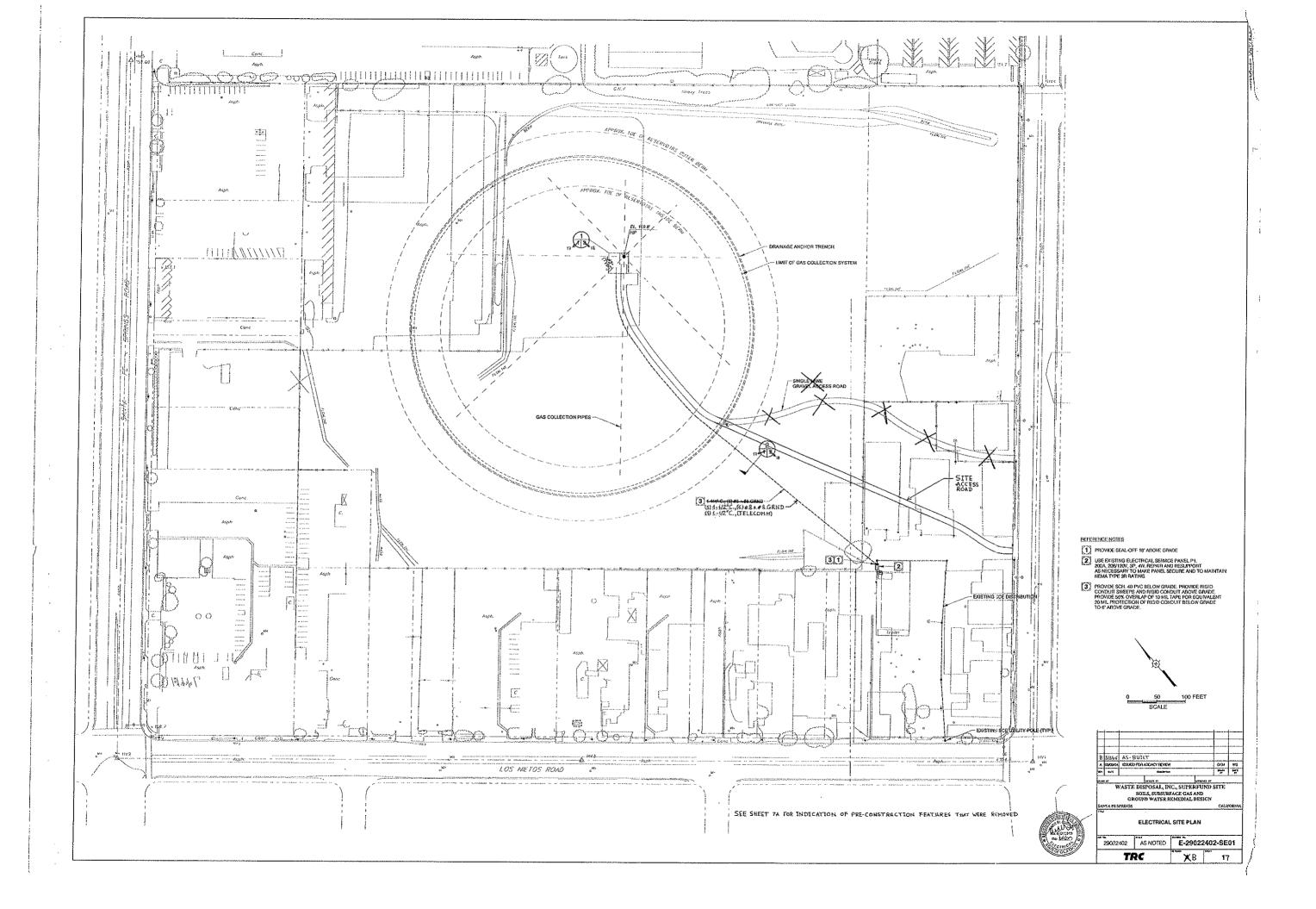


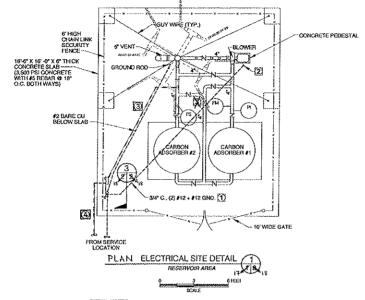












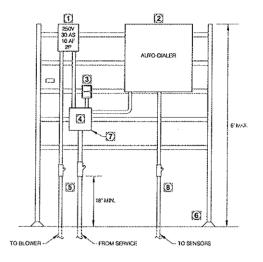
DETAIL NOTES

PROVIDE SCH. 40 PVC BELOW GRADE. PROVIDE RIGID CONDUIT 90° BENDS AND RIGID COMOUT ABOVE GROUND, PROVIDE SON OVERLAP OF 16 MIL. TAPE OR EQUIVALENT 20 MIL PROTECTION OF RIGID CONDUIT BELOW GRADE TO 6° ABOVE GRADE.

- PROVIDE 1\* CONDUIT TO SENSORS FROM AUTO-DIALER, PROVIDE BELL BOX AND SUPPORT AT STUB-UP LOCATION, ROUTE SEAL-TIGHT TO SENSOR LOCATIONS
- CONRUIT FOR LOW VOLTAGE TELECOMMUNICATION AND SIGNAL CABLES.

					F	AN	ΙĒ	L	'P	<b>'</b> 5	EE S	HEE1	ŕ	7 1	FOR PANEL PILOCAT
VOLTS: 208/120V			E: 3				A).	Ç, R	ATING:	22,000		,,	_		MAUN:200A MCB
MOUNTING: SURFACE	W	IRE	: 4												BU\$\$K4G;225A
LOAD	QTY	Ŀ	A-VA	B-YA	C VA	BKR	CT	CT	BKR	A-VA	8-VA	C-YA	T	OIX	LOAD
RECEPT - EXTERIOR	7	R	180	1995	田の合	20/1P	3	1 2	60/3P	-	15000	138000	3	_	SPARE
TRAVER SUBPANEL	1	N	25.27	3603	540. h		3	4		32560		Karan	1		
••••	1	ĪN	1999	V 330	3603	_	5	6		000034	2000	1	Т	$\vdash$	
SPACE	1	1		700 A	125215		7	B	100/20	3603	200	15000	İΝ	1	TRAILER SUSPANEL
SPACE	T	Т	100000		(18) K	-	9	110		(Asta)	3603	101180	N	_	1
SPACE:	T	П	100.00	6000			111	12	100/2P	24 11		360		1	TRAILER SUSPANEL
SPACE	1	1.		862	1448		13	14		3603	040653				1
RECEPT - EXTERIOR	11	R	to Car	400	1022	20/1P	15	16	16/2P	S. 25 (A)		13.3	ш	1	GAS EXTRACT, SLOWER HOTO
SPACE	1		33 Z G				17	18	_	(135)	35.78	410			
SPACE:	1	T		9 67 48	2370		19	20	20/1P		1	2565	1ĸ	7	GAS EXTRACT, AUTO-DIALER
SPACE	1		100,000				21	22	20/1P	91729	1200	28538	R	1	RECEPT - GAS EXTRACT, ARE
SPACE:	7	17	Sec. 20	F1327			23	124		120	28,105		m		SPACE
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	T		THE LA	QLPM.			П	1-		2033	中20gg		1		
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			7.2	j	Section			1		(20c)		22213	П		
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			X12.14	3.32			М			304	3657		17		
PHASE TOTALS:	-	~	7656	9222	7672	24530	#TC	TAL	CONNE	CTFDI	OÁD VA	IFOR I	Ϋ́	AND	LOAD SEE BELOW)
PRASE AMPERES:		╗	61.0	76.6	63.5						,		_		
DEWAND LOAD CALCULATION:		_									NOTES				
L*LIGHTING LOADS:				1.25	×	0			6	VA					
C-CONTINUOUS LOADS, OTHER:				1.25	×	ō			ō	VA		RELOC	AT	EXX	STING TRAILER SUB-FEED FROM
M-MOTOR LOADS (INCL LGST):				1.00	x	632			832	VA					7 TO CIRCUITS 3 AND 5.
LARGEST, VA:				0.25	x	632			208				•		
RERECEPTACLES: 1ST 10K:				1.00	×	1760			1750						
BALANCE:				9.50	x	0				VA					
WHITCHEN LOADS: QTY:			0	1.00	×	ŏ				VA					
N-MONCONTINUOUS LOADS, OTHE	R:			1.00	×	21918		£	21916						
P-PANEL INCL. IN ABOVE)			TOTAL	N.E.C.	DEMAND	CAOLO			24738	VA -	60.7	AME	77	es .	

LOAD SCHEDULE





#### DETAIL NOTES

- PROVIDE NEMA 3R 38A, 250V, IP FUSED DISCONNECT. PROVIDE 10A DUAL-ELEMENT TIME DELAY FUSES.
- [2] PROVIDE NEMA 3R 24' X 24' X 6" HOFFMAN ENCLOSURE FOR AUTO-DIALER ROUTE CIRCUIT AND CONNECT PER PANEL SCHEDULE.
- [3] PROVIDE WEATHER-PROOF, GIF 20A DUPLEX SERVICE RECEPTACLE OUTLET, ROUTE CIRCUIT AND CONNECT PER PANEL SCHEDULE.
- PROVIDE NEMA 3R 8" X 8" X 4" JUNCTION BOX.
- [5] PROVIDE SEAL-OFF'S ON CONDUITS EMERGING FROM BELOW GRADE.
- PROVIDE STRUT RACK, CONSTRUCT RACK WITH GALVANIZED DEEP STRUT, RACK TO BE MODERNOOM OF HENCE, PROVIDE SUPPORT STANCHIONS AND ADDITIONAL INDEPTADENT SUPPORT AS REQUIRED.
- PROVIDE AND INSTALL № AWG SOLID BARE COPPER, AND BOND TO SUAB REBAR, LOCAL FENCE, AND 58"X 10" GROUND ROD. CORREINATE GROIND ROD INSTALLATION, AT VENT RISERMANDRAM PENETTRATION WITH PROJECT MANAGERS, PROVIDE EXCITE WILD TO EACH, CONNECT TO 8 AWG GROUNDING CONDUCTOR FROM SERVICE.
- PROVIDE 1' CONDUIT TO SENSORS FROM AUTO-DIALER, PROVIDE BELL BOX AND SI/PYORY AT STUB-UP LOCATION, ROUTE SEAL-TIGHT TO SENSOR LOCATIONS.

